Optimization of Heterogeneous Arrays of Wave Energy Converters

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Background/Research Question

- The WEC dimensions are usually designed for the prevailing sea conditions in a particular location.
- Control co-design is desired.
- WEC arrays usually contain identical devices
- Can we optimize the dimensions and control to maximize the overall power absorption?
- How can we further improve performance by optimizing the number of devices in the array?





Hom. arrav Vs Het. arrav.

Dynamic Model: Spring-Mass-Damper Approximation



A simple point absorber WEC $(m + m_{\infty})\ddot{x} + C_r\dot{x} + kx = f_e - u$

- > Array dynamics $(M + M_{\infty})\ddot{\vec{x}} + C_r\dot{\vec{x}} + K\vec{x} = \vec{f}_{\rho} - \vec{u}$
- Hydrodynamic coefficients

$$M_{\infty} = \begin{bmatrix} m_{\infty 11} & \cdots & m_{\infty 1n} \\ \vdots & \ddots & \vdots \\ m_{\infty n1} & \cdots & m_{\infty nn} \end{bmatrix}$$

$$Cr_{\omega} = \begin{bmatrix} Cr_{\omega 11} & \cdots & Cr_{\omega 1n} \\ \vdots & \ddots & \vdots \\ Cr_{\omega n1} & \cdots & Cr_{\omega nn} \end{bmatrix}$$

$$q - factor = \frac{P_{array}}{N * P_{isolated}}$$





WEC Array Hydrodynamics

- We need to compute added mass, radiation damping coefficients, and excitation force coefficients.
- Boundary Element Methods tools vs. an approximate analytic method
- GA needs objective values only; qualitative conclusions on the objective values of different solutions are okay





Validation of hydrodynamics



Validation of hydrodynamics











Control Force

> The objective function:

Minimize:
$$J(u(t), x_2(t)) = \sum_{n=1}^{N} \int_{0}^{t} \{-u_n(t) * x_{2n}(t)\} dt$$

Wave



Subject to EOM:

$$\dot{\vec{x}}_{1} = \vec{x}_{2}$$
$$\dot{\vec{x}}_{2} = \frac{1}{M} \left(\vec{f}_{e}(x_{3}) - C\vec{x}_{2} - K\vec{x}_{1} - \vec{u} \right)$$
$$x_{3} = 1$$

The power constraints and control constraints:

$$\vec{u}(t) * \vec{x}_2(t) \ge -\vec{\epsilon}$$
, $|\vec{u}(t)| \le \vec{\Gamma}$





Simulation

The simulation parameters are as follows:

- Wave condition: T = 6s, H = 0.8222 m. (site: Newport, Oregon)
- (Radius and draught) Upper Bound = 10 m.
- (Radius and draught) Lower Bound = 1m.
- Hydrodynamic parameters are calculated using the approximate analytic method.
- Power from the array is computed using the constrained control PCBSB

Homogenous array result – 3 Devices



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Homogenous array result – 5 Devices



Heterogeneous array result: 3 devices



- Optimized dimensions
- *Homogeneous*: *R* = 7.2249 *m*

R1	R2	R3	р	
7.7297	6.6232	6.6095	1.0668	
7.7527	6.6143	6.6214	1.0667	

Heterogeneous array result: 3 devices



Heterogeneous array result: 5 devices



- Optimized dimensions
- Homogeneous: R = 6.1196 m

R1	R2	R3	R4	R5	р
6.6600	6.5131	6.5064	5.5635	5.5623	1.2089
6.6368	6.4822	6.4776	5.5457	5.5254	1.2087

Heterogeneous array result: 5 devices



Problem III: HGGA-Heterogenous array optimization



Hom. array Vs Het. array.

 $R_i \in [R_{min}, R_{max}], D_i \in [D_{min}, D_{max}], N \in [1, N_{homogenous}]$

 $Total Vol. of Het array \leq Total Vol. of Hom. array.$



GA flow chart.





Hidden Genes GA (HGGA)

R1

HGGA

A variation on GA that allows optimizing the number of design variables, simultaneously with the variables.

T1 T2 T3 T4 D1 D2 D3 D4 R2 R3 R4 0 0 D1 R2 D2 D3 **R4** R3 **R1 D4**

Example of 4 WECs

- A maximum of 4 WECs
- Variables: Radius R1 R4, Draughts D1 D4, and tags.

Homogeneous Array from literature

- Test case from Giassi 2018.
- R = 2 m, draft d = 0.5 m, and water depth h = 25 m.
- Wave site in Lysekil on the Swedish west coast.



- Regular wave, wave height H = 1.53 m, period T = 5.01 s.
- Wave propagating along the x-axis.

$$Maximize: p = \frac{P_{heterogeneous}}{P_{homogeneous}}$$

HGGA-Heterogeneous array result



Conclusion

- Investigated increasing power by allowing devices of different dimensions in the same array.
- Could allow the number of devices to vary during optimization
- Heterogenous arrays can produce more power while reducing total volume of buoys.

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Questions

Semi-analytic hydro coefficients

- > In the whole fluid domain, the governing equation $\nabla^2 \phi = 0$
- Boundary conditions:
 - Free surface boundary conditions

> Seabed condition
$$\left. \frac{\partial \phi}{\partial z} \right|_{z=-d} = 0$$

Impermeable surface condition on the body surface

$$\frac{\partial \phi}{\partial r} = 0, (r = a, -h \le z \le 0), \frac{\partial \phi}{\partial z} = 0, (0 \le r \le a, z = -h)$$

Summerfeld radiation condition

$$\lim_{x \to \infty} \sqrt{r} \left(\frac{\partial \phi}{\partial r} - ik_n \phi \right) = 0$$

 $\omega^2 \phi - g \frac{\partial \phi}{\partial z} \Big|_{z=0} = 0$

Radiation: exterior potential functions



Radiation: Interior potential functions

- Based on the methods of variable separation and matching eigenfunction expansion for the velocity potential.
- > Separation of variables : $\emptyset_{3,m}^{I}(r,z) = \emptyset_{3,h}^{I} + \emptyset_{3,p}^{I}$
- The homogenous potential function

$$\emptyset_{3,h}^{I} = \frac{C_{R0}}{2} \left(\frac{r}{a}\right)^{m} + \sum_{n=1}^{\infty} C_{Rn} \frac{I_m \left(\frac{n\pi r}{(d-h)}\right)}{I_m \left(\frac{n\pi a}{(d-h)}\right)} \cos\left(\frac{n\pi z}{(d-h)}\right)$$

The particular solution

$$\phi_{3,p}^{I} = \frac{1}{2(d-h)} \left[(z+d)^{2} - \frac{r^{2}}{2} \right]$$

Continuity conditions

- In both the radiation and diffraction problems, the matching conditions represent the continuity of mass flux, pressure and normal velocity.
- > The velocity potentials between interior and exterior domains are matched at the imaginary boundary (r = a).

- > The unknown Fourier coefficients C_n , D_n , C_{Rn} , D_{Rn} are solved using the matching conditions.
- The hydrodynamic coefficients are found by integrating the potential functions over their corresponding area.