



# Passive control for wave energy systems: An overview

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1. Motivation: Why passive control? Reactive vs. Passive control strategies
2. Brief review: Passive control approaches
3. Waveston: Passive control with real industrial relevance
4. Open research challenge: Waveston passive control (WAPPAC) competition

Motivation: Why passive control?  
Reactive vs. Passive control strategies

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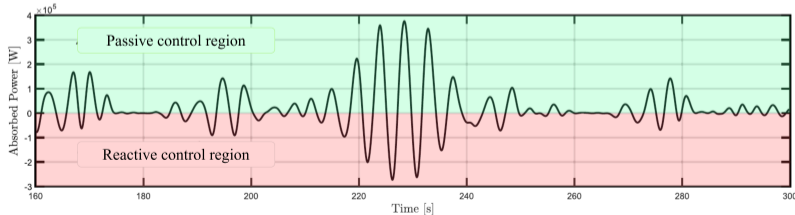
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**Change of control objective paradigm:**

For many years, WEC control objective focused on **maximising** absorbed energy, leading to **reactive** control strategies, often positioning passive control as a lower-performance approach.

- Reactive control can potentially achieve **high energy absorption** relying on:
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**More recently**, control objective has shifted towards a **techno-economic perspective**, where **energy production** is assessed jointly with **CapEx** and **OpEx** to reduce the levelised cost of energy (**LCoE**).

$$\min. \quad LCoE = \frac{CapEx + OpEx}{E}$$

Within this evolving **techno-economic** context:

**Limitations of reactive control:**

**Why passive control matters:**

Within this evolving **techno-economic** context:

## Limitations of reactive control:

- **Increased** device motion and PTO forces, may **accelerate** structural fatigue **increasing** OpEx.

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However, while passive control may appear conceptually simpler and beneficial in the broader techno-economical context, the **nonlinear passivity (power) constraint** poses a significant **challenge** for both control design and real-time implementation.

## Brief review: Passive control approaches

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The energy-maximising **passive control problem** is typically formulated as follows:

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$$p_{pto}(t) = f_{pto}(t) x_2(t) \leq 0$$

- Passivity: mixed control-state nonlinear (NL) constraint, **nonconvex** in the general case.
- Potentially **quadratic** objective function (OF).

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## Passivity constraint: Main consequences

Enforcing **passivity** leads to **nonconvex** OCP and potentially **NL** dynamics, thus **challenging** the design of computationally efficient control schemes.

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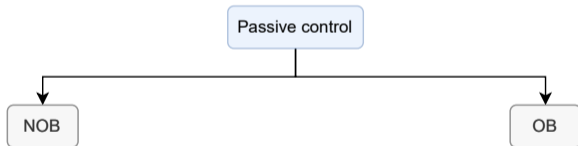
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## Passive control main challenge:

**Design** a control strategy that **balances** the **trade-off** between: **power absorption performance** & **computational cost**, while respecting the WEC physical **constraints**.

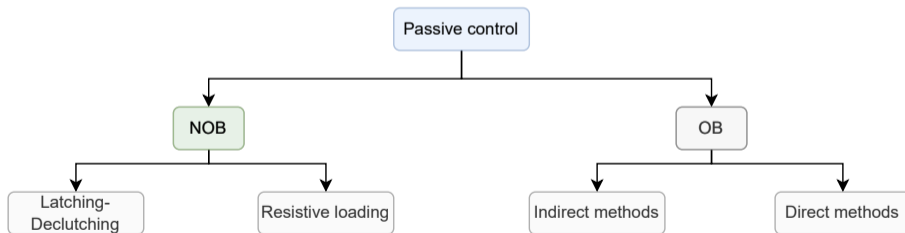
To address the main challenges, different passive control approaches have been proposed in wave energy literature, broadly **categorised** as:

- **Non-optimisation-based (NOB) control:**  
(based on fundamental understanding of the problem hydrodynamics to design the control)
- **Optimisation-based (OB) control:**  
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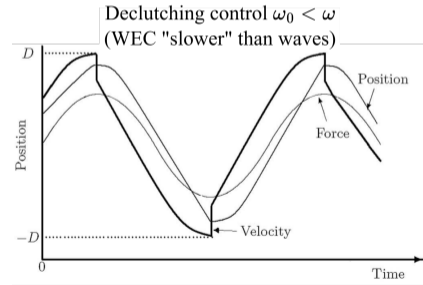
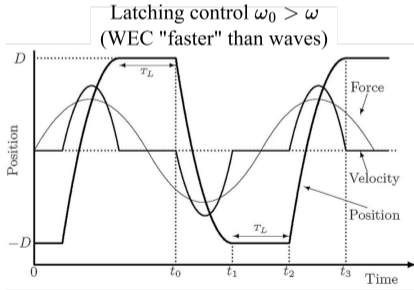
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Non-optimisation-based (NOB)

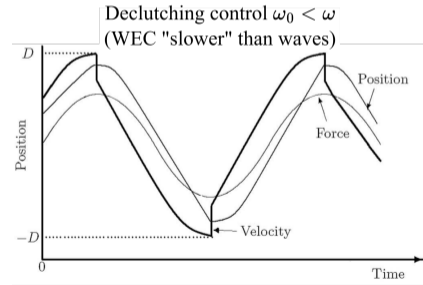
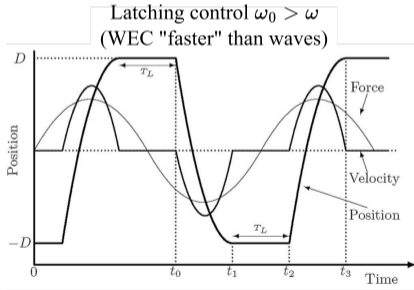
**Latching** and **declutching** constitute **early approaches** of **passive control strategies**.

- Both exploit classical wave energy theory: WEC response is shaped so that the **velocity** of the device is **in phase** with the **wave excitation force** (well-known **impedance matching** result) [1, 2].



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- Control problem usually reduces to compute the optimal **latching-declutching times**.



**Resistive loading** implements a **structured** PTO force  $f_{pto}(t) = -B_{pto}(t) \dot{x}_2(t)$ , where the **damping** coefficient is defined by exploiting the **impedance-matching** result:

$$B_{pto}(t) = |Z_w(j\omega)| = \sqrt{B_r^2(\omega) + (\omega(m_w + A_r(\omega) - S_h/\omega))^2}, \quad \omega = \begin{cases} \{\omega_e, \omega_{pk}\} \rightarrow \text{constant}, \\ \hat{\omega}(t) \rightarrow \text{time-varying}. \end{cases}$$

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**NOB controllers:**

## Benefits

Simple concept & real-time implementation.

## Drawbacks

- (i) Inherently **suboptimal**.
- (ii) Do not contemplate WEC **constraints** in the control definition.
- (iii) Latch-Decel strategy extension to **polychromatic** sea states is not straightforward.

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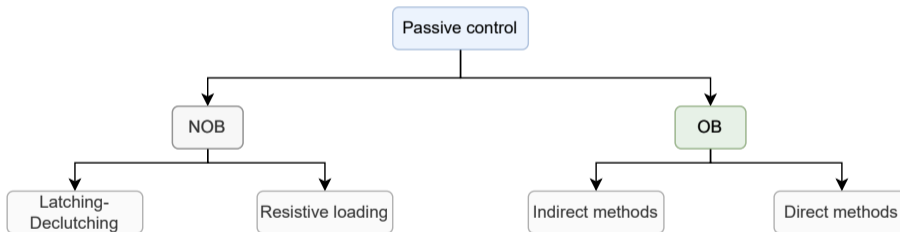
Optimisation-based (OB)

## OB Indirect methods

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### (OB) Indirect methods

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- **Formulation:** Optimality conditions derived via PMP, then discretised to solve the BVP.

### (OB) Direct methods

(First discretise, then optimise)

- **Formulation:** OCP transcribed into a NLP, then solved via KKT conditions.

Although **both** indirect and direct methods are **viable** for wave energy systems, **indirect** approach present various **implementation difficulties** compared to **direct** methods [3, 4].

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- **Numerical robustness:** BVP presents high sensitivity to **costate** (non-physical vars.) **initialisation**, possible **ill-conditioned** or **unstable costates dynamics**.

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OB Direct methods approach: **First discretise, ...**

**Unstructured OCP:**

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- **Reactive control:** NLP is usually a **QP** and **KKT** left-hand-side **matrix gradients** are **constant**: do not depend on current iteration of  $\tilde{w}$ .

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**Passive control:** **nonconvex** NLP & **gradients** in the **KKT** matrix explicitly **depend** on **current iteration**  $\tilde{w}$ , yielding **much more computationally demanding** NLP problems to solve.

How can we estimate the **computational cost** of solving NLP problems? It is mainly determined by **two components** [3, 5]:

$$T_{\text{iter}} \approx T_{\text{LA}} + T_G$$

- (i) **Linear algebra cost:** solving the KKT system at each iteration:

**Linear KKT sys. (SQP & IP)**



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- (ii) **Gradients evaluation cost:** computation of KKT sys. **elements**.

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(i) **Linear algebra cost:** solving the KKT system at each iteration:

- **Dimension** of the KKT system, 
- **Sparsity** pattern and nnz elements **ordering** in KKT matrix, 

**Linear KKT sys. (SQP & IP)**



$$\begin{bmatrix} \nabla^2 \mathcal{L}(\tilde{w}) & \nabla c(\tilde{w})^\top \\ \nabla c(\tilde{w}) & \mathbf{0} \end{bmatrix} \begin{bmatrix} \Delta \tilde{w} \\ \Delta \lambda \end{bmatrix} = - \begin{bmatrix} \nabla \tilde{J}(\tilde{w}) \\ c(\tilde{w}) \end{bmatrix},$$

(ii) **Gradients evaluation cost:** computation of KKT sys. **elements**.

How can we estimate the **computational cost** of solving NLP problems? It is mainly determined by **two components** [3, 5]:

$$T_{\text{iter}} \approx T_{\text{LA}} + T_G$$



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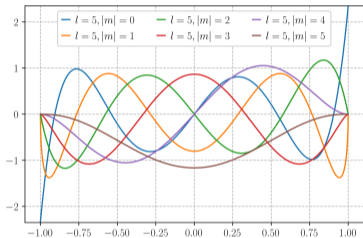
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KKT sys. **Dimension & Sparsity** ( $T_{\text{LA}}$ ) depend on: (i) **discretisation method**, and (ii) **NLP formulation**.

(i) How the **discretisation** method influences the **computational cost**:

**Global support, pseudospectral (PS):**

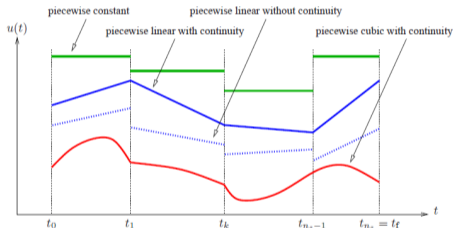
(Fourier - HRCF - Legendre)



- **Global domain:** overall horizon.
- **Strong coupling:** Each decision var. influences the solution everywhere.

**Compact support:**

(ZOH - FOH)



- **Local domain:** interval-wise.
- **Local coupling:** Each decision var. influences only neighbours.

(i) How the **discretisation** method influences the **computational cost**:

**Global support, pseudospectral (PS):**

(Fourier - HRCF - Legendre)

- **Dense** representation 

**Compact support:**

(ZOH - FOH)

- **Sparse** representation. 

Generic **NLP**:

$$\max. \tilde{J}(\tilde{w}) = A_1 \tilde{w} + B_1 q_1(\tilde{w})$$

$$\text{s.t. } c_L \leq c(\tilde{w}) = A_2 \tilde{w} + B_2 q_2(\tilde{w}) \leq c_U,$$

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**Global support, pseudospectral (PS):**

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- **Dense** representation 
- **Convergence:** spectral for smooth signals  $\Rightarrow$  less nodes  $\Rightarrow$  dimension drops 

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- **Sparse** representation. 
- **Convergence:** algebraic  $\Rightarrow$  more nodes  $\Rightarrow$  dimension rises 

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(ii) How the **NLP formulation** influences the **computational cost**. There are **two** main formulations:

## Simultaneous:

- **Full discretisation: states & inputs**  
(control-wave excitation)

## Sequential:

- **Only inputs are discretised** (control-wave excitation)


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## Simultaneous:

- **Full discretisation: states & inputs** (control-wave excitation)
- **Particular case:** for linear dyn., **states** can be **cancelled** analytically  $\Rightarrow$  **condensed** NLP in terms of **control vars. only**.

## Sequential:

- **Only inputs** are **discretised** (control-wave excitation)
- **Particular case:** for linear dyn., closed-form solution can be used to **cancel** the **states** (exact discretisation)  $\Rightarrow$  **condensed** NLP in terms of **control vars. only**.

While **condensing** significantly **reduces** the **dimension** of the NLP () , and is the standard approach for **reactive control**, the implications for **passive control** are **different...**

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**Passive control:** KKT matrix gradients explicitly depend on the current iterate  $\tilde{w}$ .

- KKT matrix needs **re-computation** and **re-factorisation** at every iteration (↑).

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Condensing in general is **less attractive** for WEC problems with nonlinear passivity constraints (compared to the reactive control case).

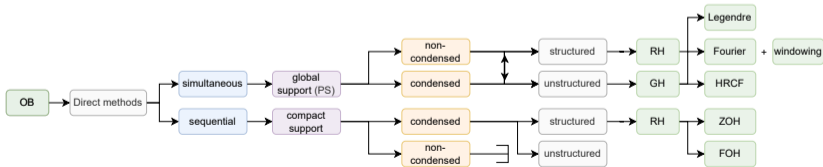
Several direct method approaches have been developed in literature:

- SIM(n-cond & cond)-**GHPSC**(Fourier,Legendre)-uns.NLC [6, 7, 8, 9, 10].
- SIM(cond)-**RHPSC**(Fourier + windowing) (implemented for reactive control) [11, 12].
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**Open-question:** Which is the **most suitable direct** optimal control scheme—comprising OCP **discretisation** and **NLP formulation**—for **passive** control of wave energy systems, **balancing** the trade-off between power absorption, computational cost, constraint satisfaction, and modelling fidelity?

# Wavepiston: Passive control with real industrial relevance

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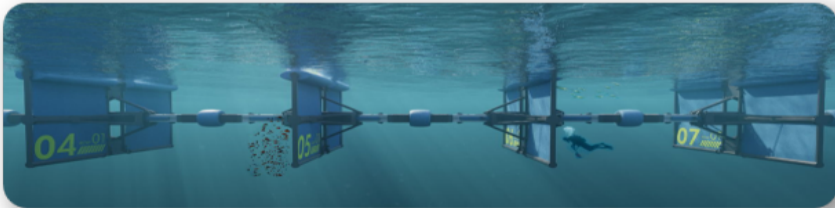
Passive control strategies are not only a interesting control exercise, but it began to have **real industrial applications**.

## Wavepiston: From passive OCP to a real case scenario.

Passive control strategies are not only a interesting control exercise, but it began to have **real industrial applications**.

### Wavepiston vision and the role of passive control:

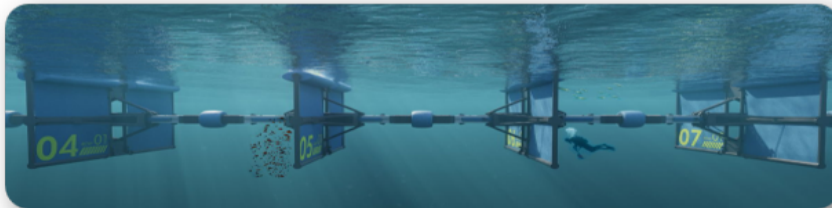
- **Wavepiston technology development:** is driven by a **strong focus** on **minimising LCoE** seeking for simplicity, reliability, and scalability.



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## Wavepiston vision and the role of passive control:

- **Wavepiston technology development:** is driven by a **strong focus** on **minimising LCoE** seeking for simplicity, reliability, and scalability.
- The use of a **passive PTO** is a deliberate **design choice**.
- Therefore, **passive control** strategies constitute a **central** element of Wavepiston philosophy.



Open research challenge: Wavepiston  
passive control (WAPPAC) competition

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The **WavePiston Passive Control (WAPPAC)** competition is an open research challenge offered to the wave energy and control communities:

- **Participants:** invited to design passive control strategies for the Wavepiston device.
- **Objective:** minimise LCoE-surrogate, while respecting the PTO passivity constraint.

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**Competition purpose:** foster collaboration across the wave energy and control communities to advance the state-of-the-art in passive control through a realistic, industry-relevant case study.

# Thank you!




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Taighde Éireann  
Research Ireland



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 [coer.maynoothuniversity.ie/19](https://coer.maynoothuniversity.ie/19)

## References

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- [1] B. Teillant et al. “*Optimal Damping Profile for a Heaving Buoy Wave Energy Converter*”. In: *IFAC Proceedings Volumes 43 (20 Sept. 2010)*, pp. 360–365. ISSN: 14746670. DOI: 10.3182/20100915-3-DE-3008.00067.
- [2] A. Babarit and A. Clément. “*Optimal latching control of a wave energy device in regular and irregular waves*”. In: *Applied Ocean Research 28 (2 Apr. 2006)*, pp. 77–91. ISSN: 01411187. DOI: 10.1016/j.apor.2006.05.002. URL: <https://linkinghub.elsevier.com/retrieve/pii/S0141118706000423>.
- [3] J. T. Betts. *Practical Methods for Optimal Control and Estimation Using Nonlinear Programming*. Society for Industrial and Applied Mathematics, Jan. 2010. ISBN: 978-0-89871-688-7. DOI: 10.1137/1.9780898718577.

# References

- [4] B. Chachuat. *Nonlinear and Dynamic Optimization: From Theory to Practice*. 2007. URL: <https://infoscience.epfl.ch/handle/20.500.14299/12332>.
- [5] L. T. Biegler. *Nonlinear Programming*. Society for Industrial and Applied Mathematics, Jan. 2010. ISBN: 978-0-89871-702-0. DOI: 10.1137/1.9780898719383.
- [6] F. Paparella and J. V. Ringwood. “Receding Horizon Pseudo-Spectral Control for Energy Maximization of a 1/25th Scale Hinge-Barge Wave Energy Converter”. In: *Proceedings of the 12th European Wave and Tidal Energy Conference*. Sept. 2017.
- [7] A. Merigaud and J. V. Ringwood. “Improving the Computational Performance of Nonlinear Pseudospectral Control of Wave Energy Converters”. In: *IEEE Transactions on Sustainable Energy* 9 (3 July 2018), pp. 1419–1426. ISSN: 1949-3029. DOI: 10.1109/TSTE.2017.2786045.
- [8] L. Wang and J. Isberg. “Nonlinear Passive Control of a Wave Energy Converter Subject to Constraints in Irregular Waves”. In: *Energies* 8 (7 June 2015), pp. 6528–6542. ISSN: 1996-1073. DOI: 10.3390/en8076528.

# References

- [9] J. K. Jain et al. “Limiting reactive power flow peaks in wave energy systems”. In: *IFAC-PapersOnLine* 55 (31 2022), pp. 427–432. ISSN: 24058963. DOI: 10.1016/j.ifacol.2022.10.465.
- [10] E. M. Gelos et al. “Influence of Restoring Force Absence and Passive Power Take-Off on WavePiston Performance”. In: *Proceedings of the European Wave and Tidal Energy Conference 16 (Sept. 2025)*. ISSN: 2706-6940. DOI: 10.36688/ewtec-2025-964.
- [11] A. Mérigaud and J. V. Ringwood. “Towards realistic non-linear receding-horizon spectral control of wave energy converters”. In: *Control Engineering Practice* 81 (Dec. 2018), pp. 145–161. ISSN: 09670661. DOI: 10.1016/j.conengprac.2018.08.024.
- [12] C. Auger et al. “Receding-Horizon Pseudo-spectral Control of Wave Energy Converters Using Periodic Basis Functions”. In: *IEEE Transactions on Sustainable Energy* 10 (4 Oct. 2019), pp. 1644–1652. ISSN: 1949-3029. DOI: 10.1109/TSTE.2018.2868546. URL: <https://ieeexplore.ieee.org/document/8454324/>.

- [13] J. K. Jain et al. “Optimal Control of Wave Energy Devices with Nonlinear Reactive Power Constraints”. In: *IFAC-PapersOnLine* 55 (16 2022), pp. 98–103. ISSN: 24058963. DOI: [10.1016/j.ifacol.2022.09.007](https://doi.org/10.1016/j.ifacol.2022.09.007).
- [14] D. Montoya et al. “Passive Model Predictive Control on a Two-Body Self-Referenced Point Absorber Wave Energy Converter”. In: *Energies* 14 (6 Mar. 2021), p. 1731. ISSN: 1996-1073. DOI: [10.3390/en14061731](https://doi.org/10.3390/en14061731).