



**PAMEC 2024**  
Barranquilla – January 22<sup>nd</sup>

# Review of Dalhousie University's Past and Current Projects on Numerical Modelling of Tidal Turbines and Load Characterization

**Dr. Dominic Groulx and Abiola Akinnibosun**  
Mechanical Engineering, Dalhousie University

# Introduction

- Dalhousie University, with its proximity to the Bay of Fundy, the largest tidal reservoir in the world, aims to develop expertise in the field of Tidal Power engineering.
- One of the long term goal of Dalhousie Engineering CFD research is to develop expertise in “Fundy” high flow environment:
  - Turbulent modeling
    - turbines, other devices;
  - Wake study;
  - Turbine arrays.

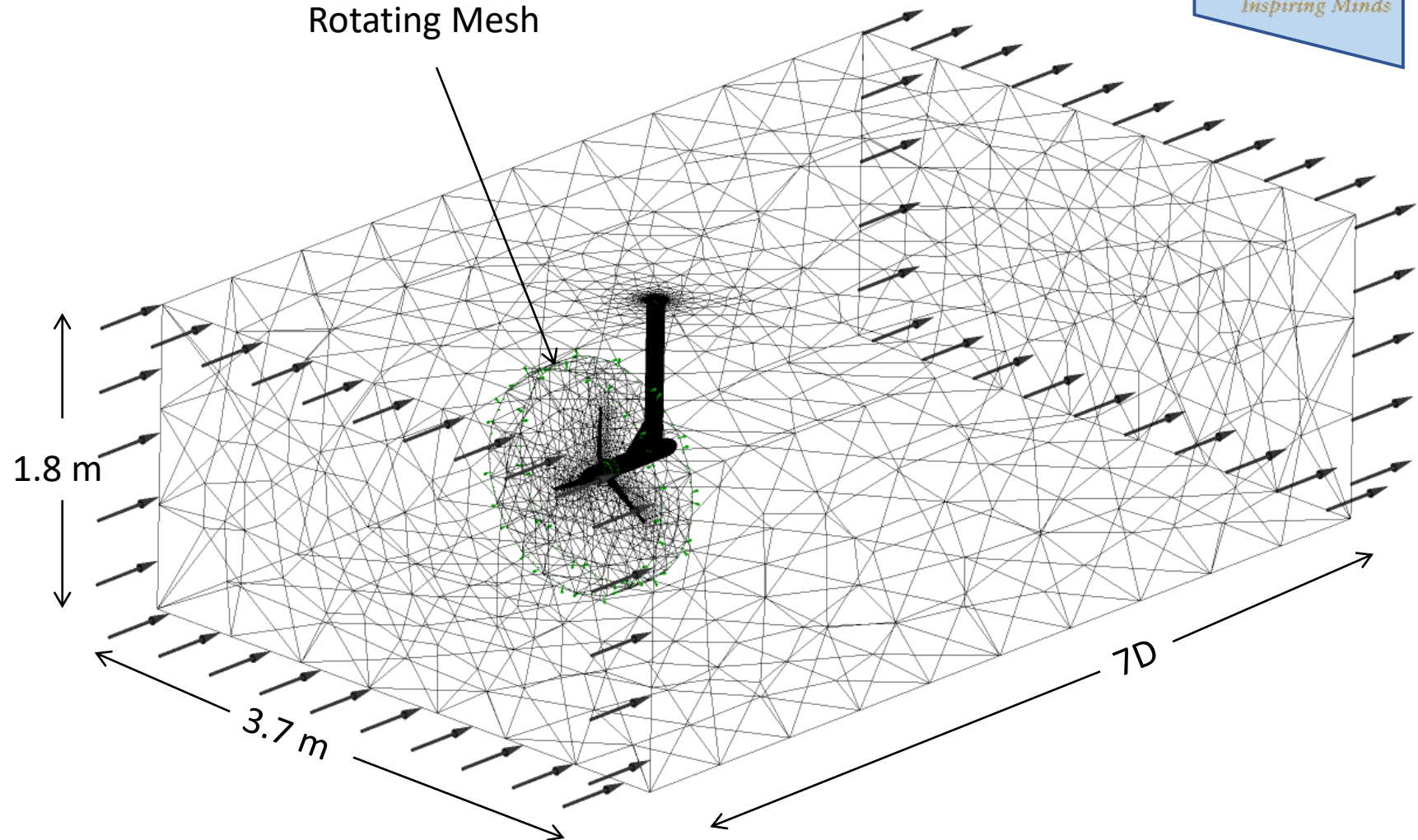


# Work Done – Osbourne (2014)

- ANSYS CFX
- Steady state, SST
- Rotating mesh
- 2D upstream, 5D downstream

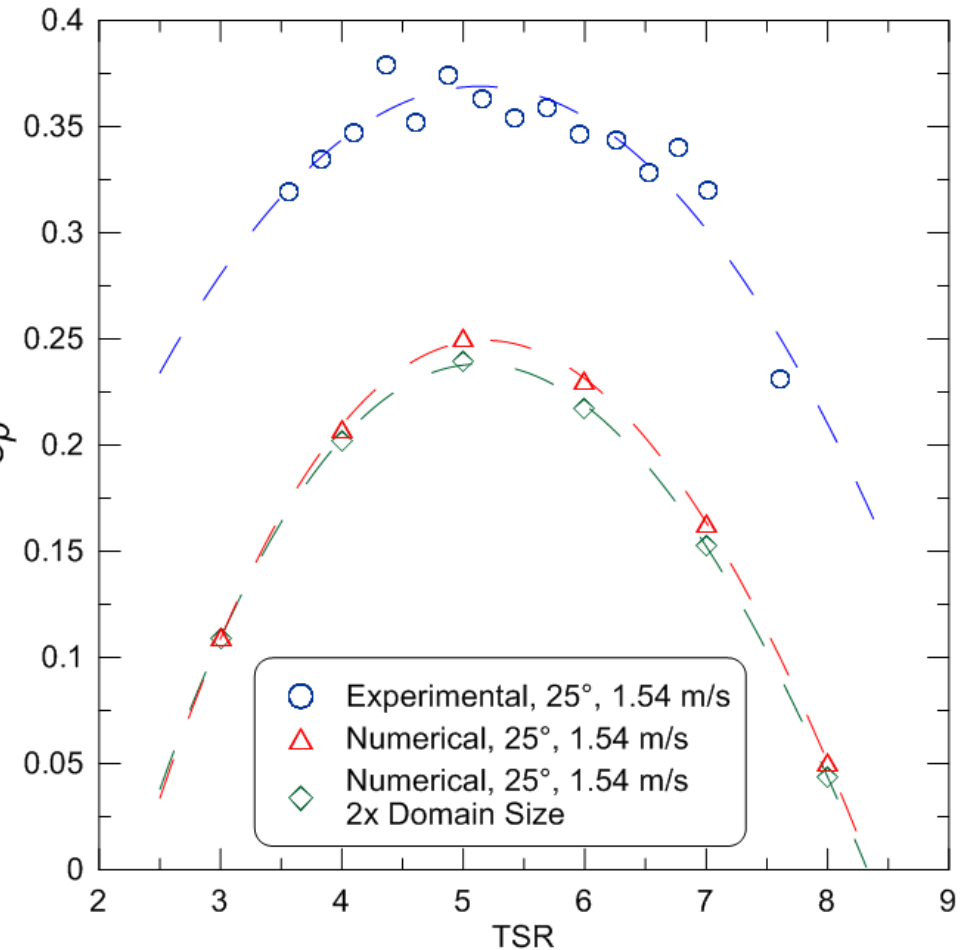
## Boundary Conditions

Boundary	Condition
Inlet	Normal Speed (1.54 m/s)
Outlet	$P_{rel} = 0$ Pa
Outer Walls	Free-Slip Condition
Turbine Walls	No-Slip Condition
Domain Interfaces (Steady State)	Frozen Rotor
Inlet Turbulence Intensity	5%



# Experimental Comparison

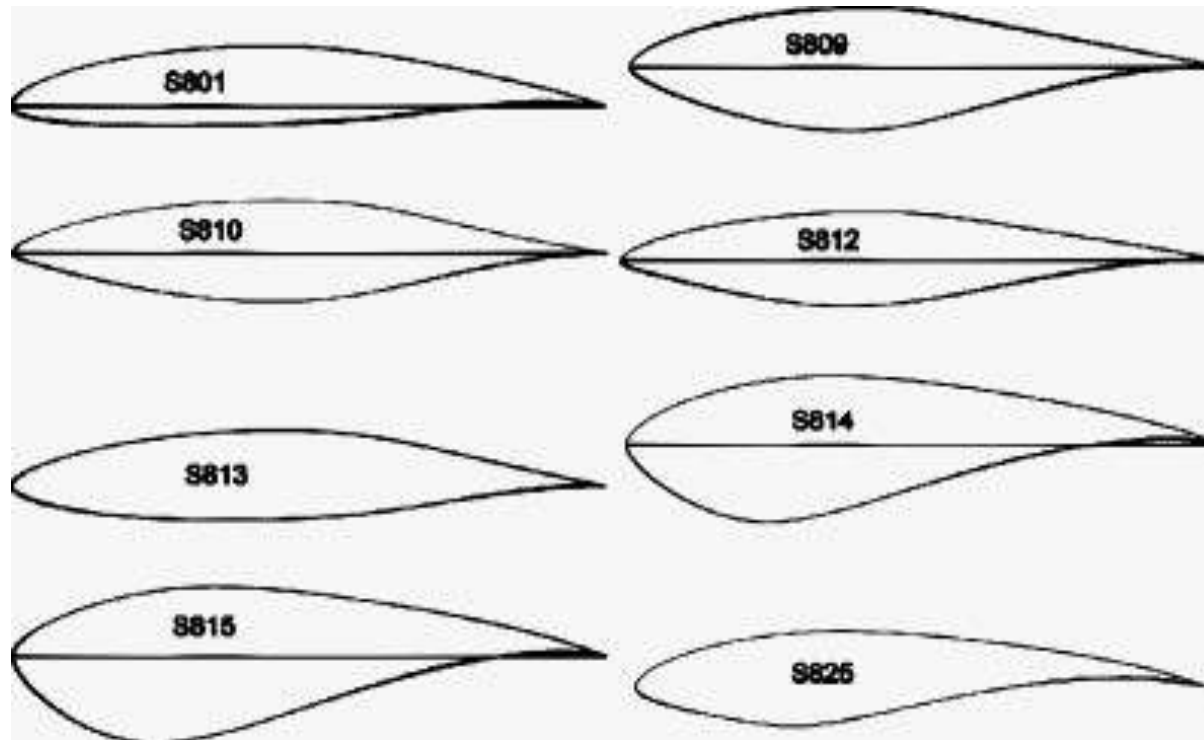
- General trend is observed but power coefficient is under-predicted. Peak of 0.25 at TSR = 5
  - Relative difference of 48% with average absolute difference of 0.14
- Increased domain size by factor of 2
  - Reduced power coefficient by additional 6% of original numerical result



# Introduction

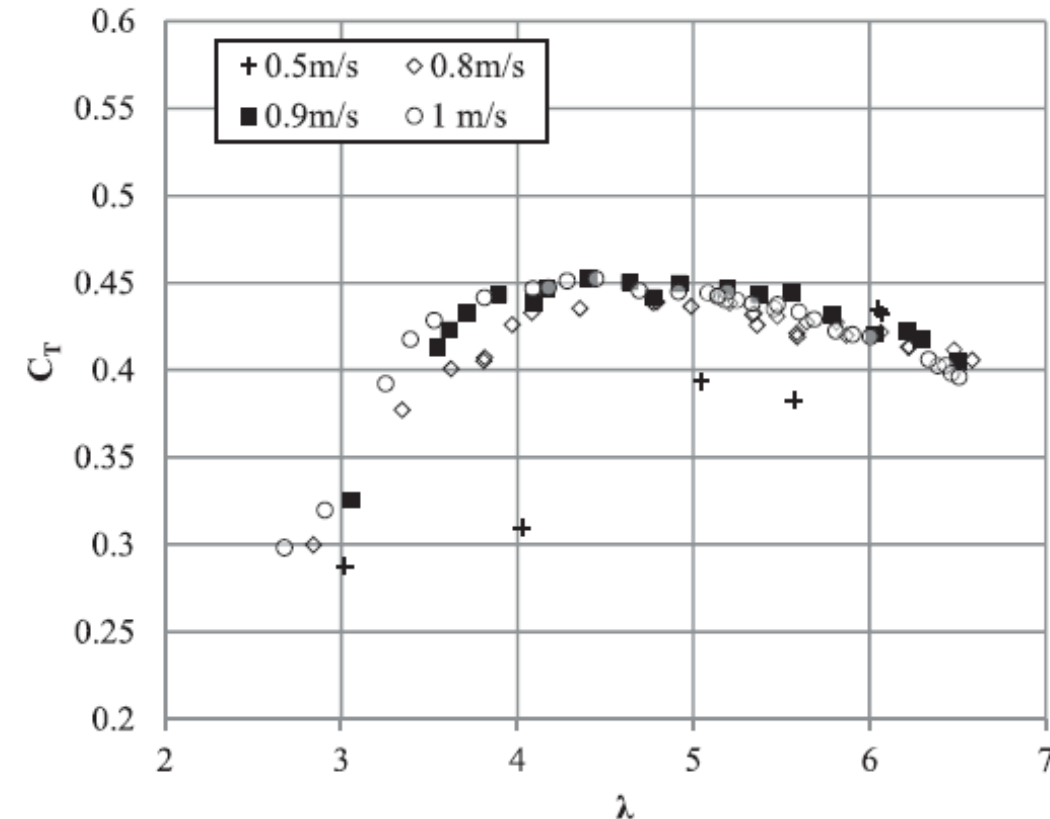
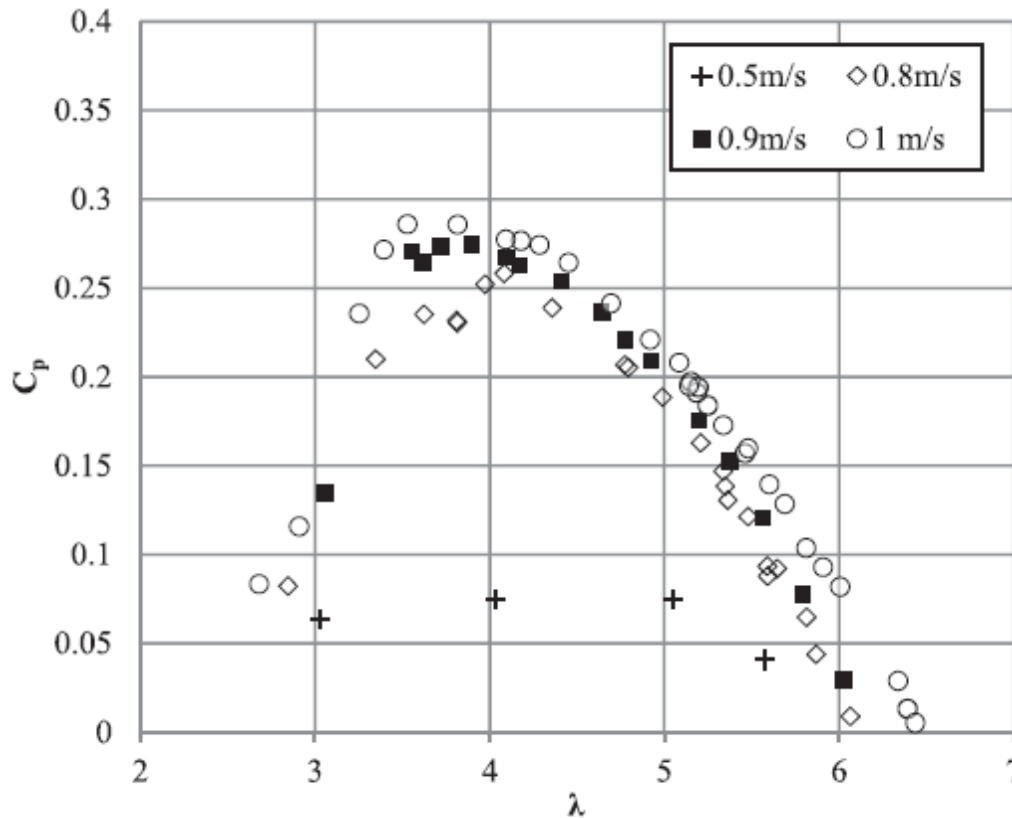
Researchers at Dalhousie and Strathclyde have been working on passively adaptive rotor blade for horizontal-axis tidal turbine using the bent-twist properties of composite materials.

The selected blade profile used for the study was the NREL S814



# Introduction

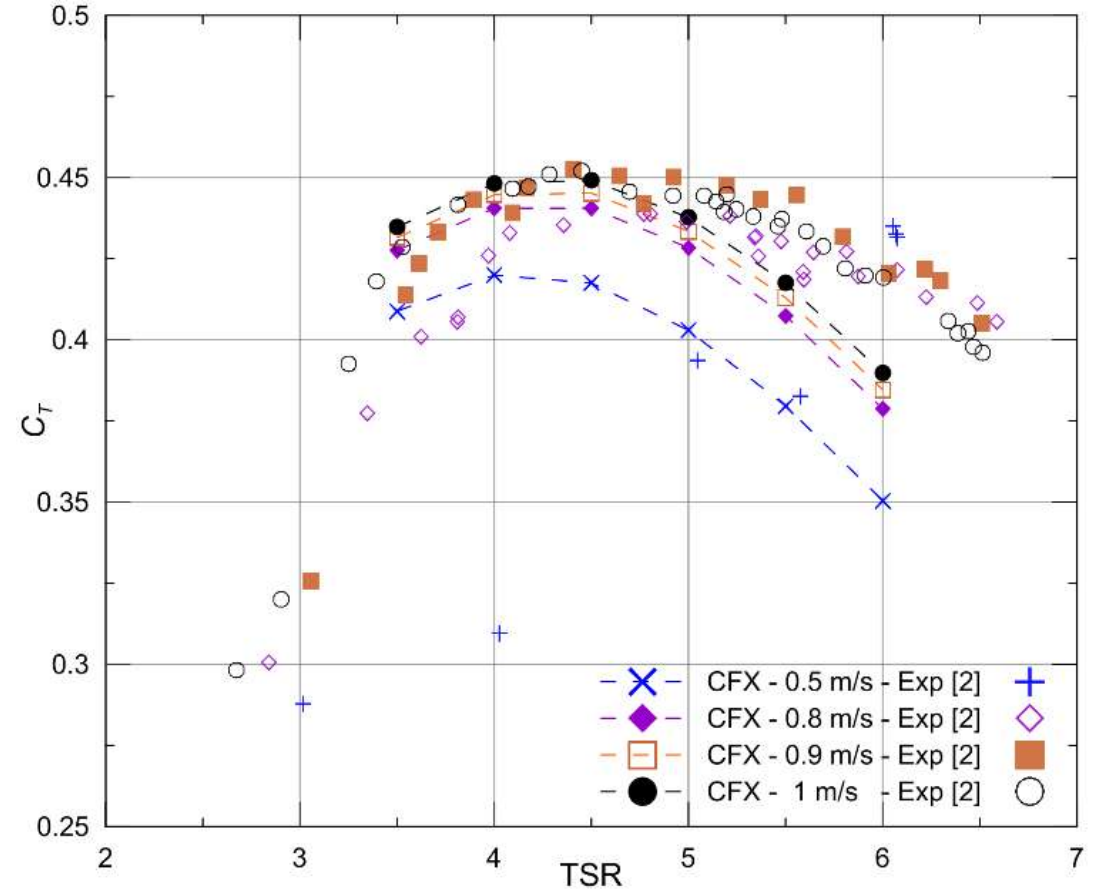
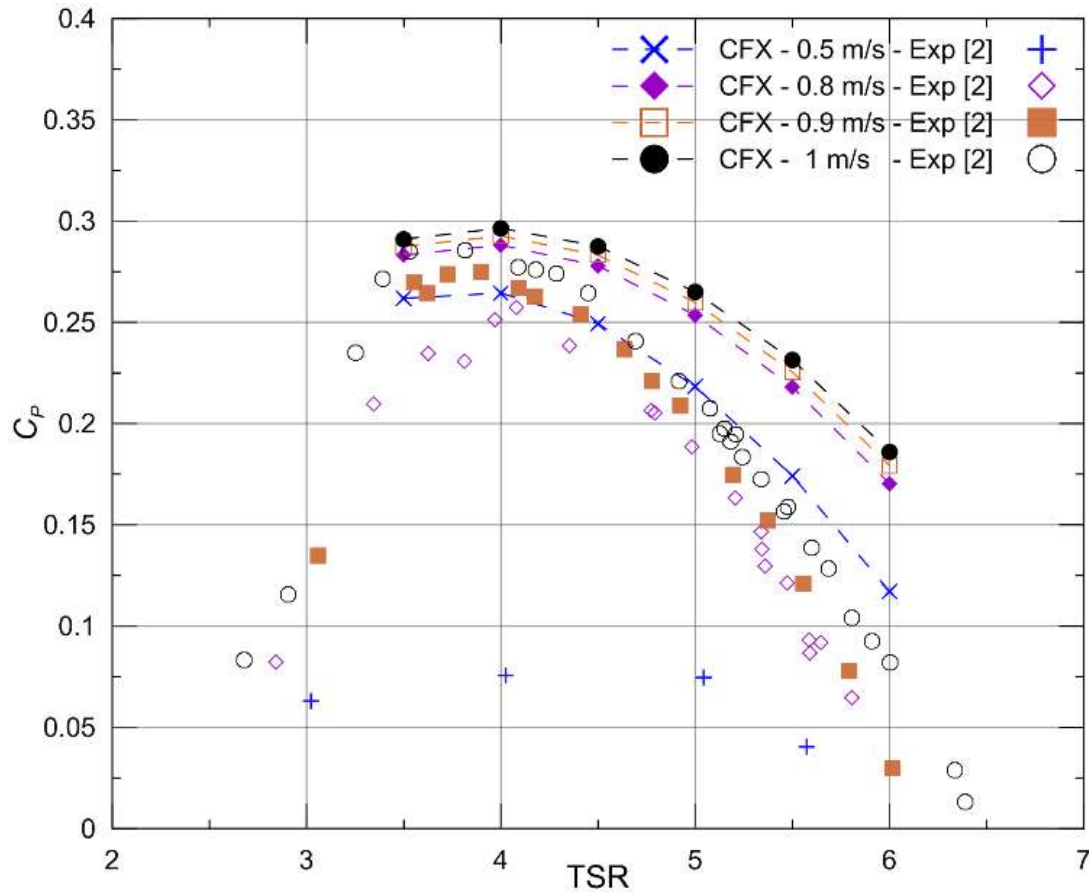
As part of the project, a first series of tow tank tests, at 1/20<sup>th</sup> scale, was performed using rigid blades at Strathclyde's Kelvin Hydrodynamics Laboratory tow tank.



D.A. Doman, R.E. Murray, M.J. Pegg, K. Gracie, C.M. Johnstone, T. Nevalainen (2015) Tow-tank testing of a 1/20<sup>th</sup> scale horizontal axis tidal turbine with uncertainty analysis, *International Journal of Marine Energy*, 11, pp. 105-119



# Comparison to Experimental



G. Currie, N. Osbourne, D. Groulx (2016) Numerical Modelling of a Three-Bladed NREL S814 Tidal Turbine, *3<sup>rd</sup> Asian Wave and Tidal Energy Conference (AWTEC)*, 10 p.



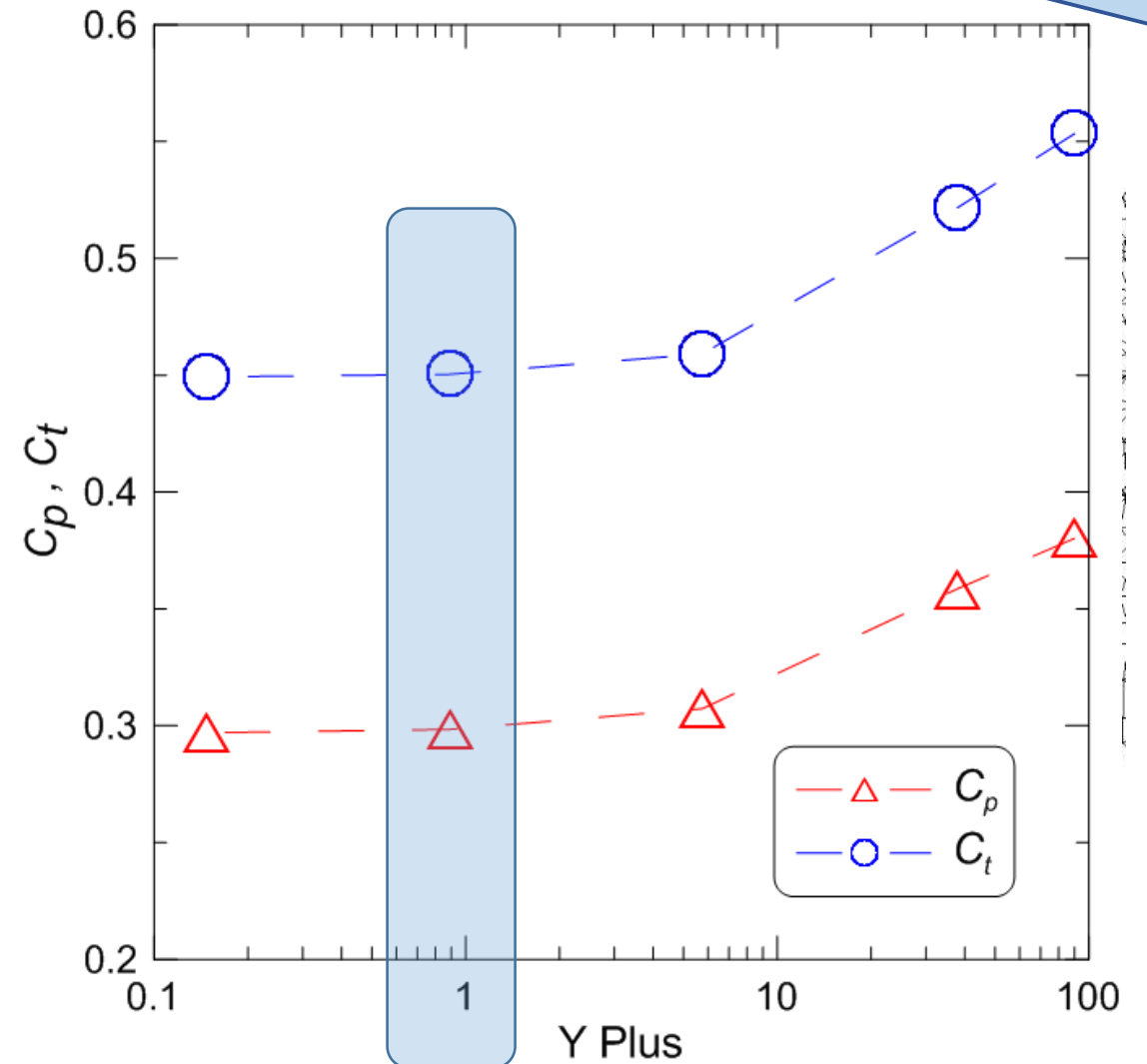
# Wake Mesh Convergence Study

Inflation layers were used;  $y^+$ :

$$y^+ = \frac{\Delta y_p}{\nu} \sqrt{\frac{\tau_w}{\rho}}$$

where  $\Delta y_p$  is the distance between the first and second grid points off the wall,  $\nu$  is the fluid's kinematic viscosity,  $\tau_w$  is the wall shear stress and  $\rho$  is fluid density.

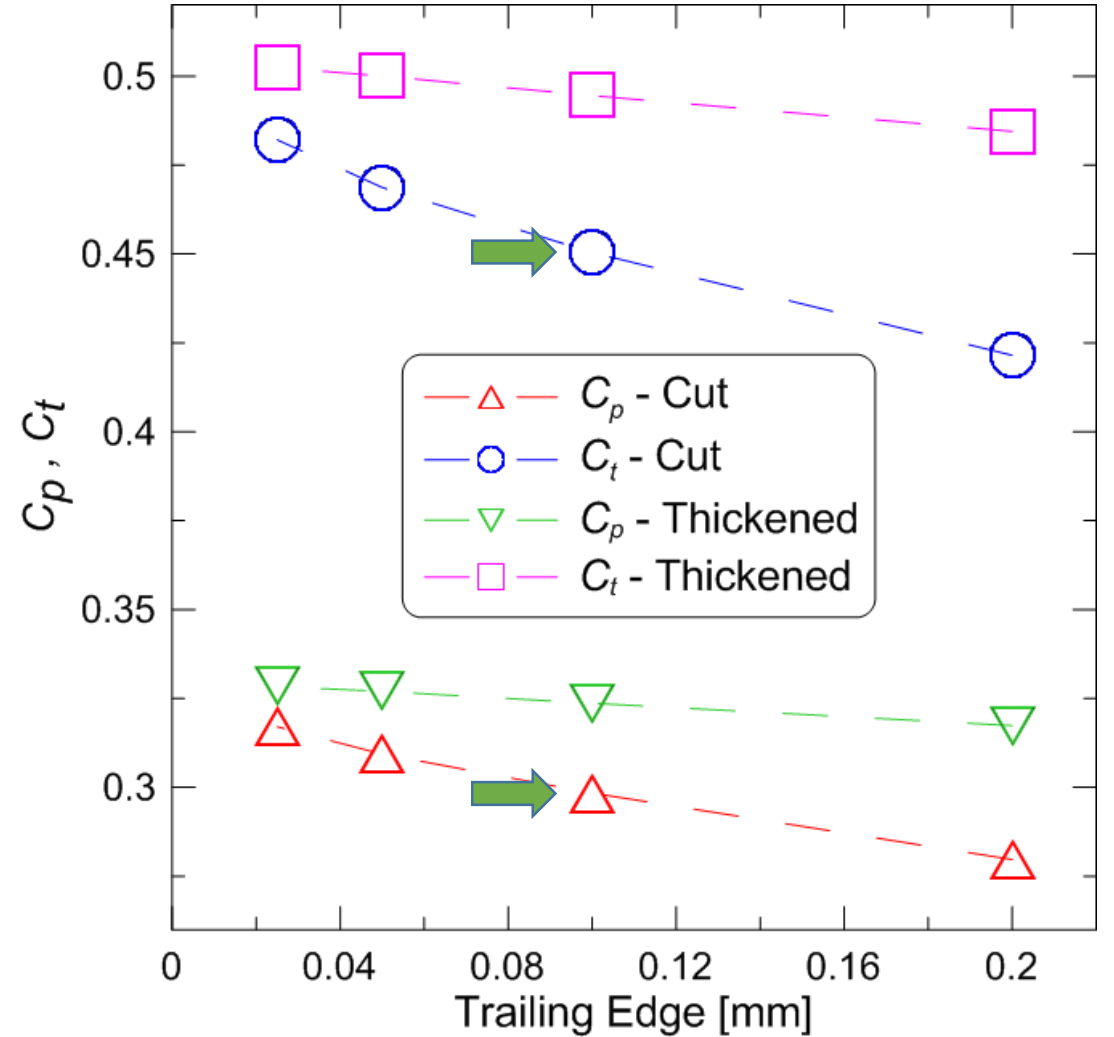
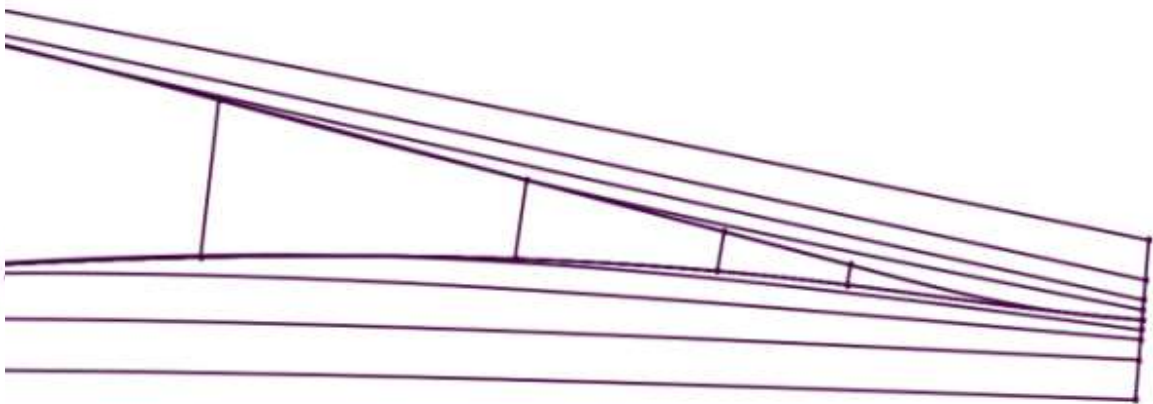
The baseline mesh contained a maximum global  $y^+ < 11$  ensuring the first nodes are within the laminar sublayer and that the near wall flow is resolved instead of using wall functions.





# Wake Mesh Convergence Study

Trailing edge effect



# Wake Mesh Convergence Study

Now looking at the wake

$$V_{deficit} = 1 - \frac{V_W}{\bar{V}}$$

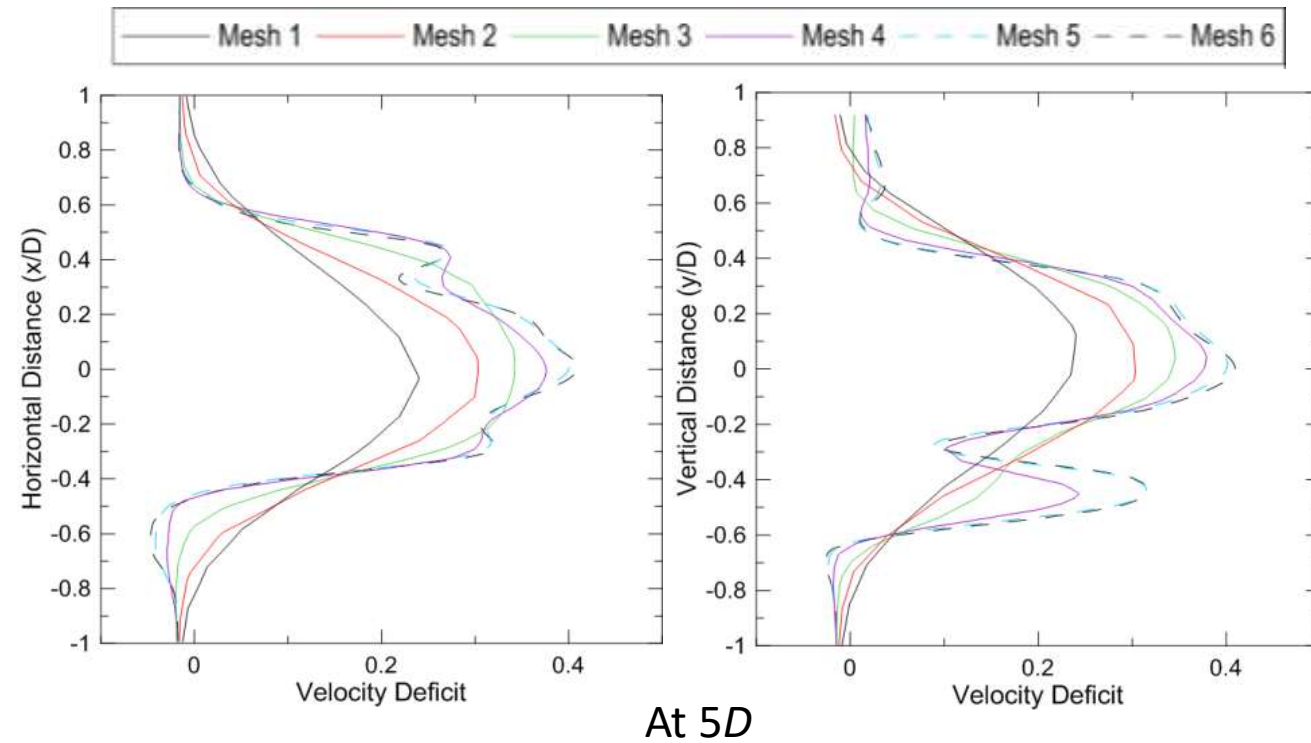
with  $V_W$  is the local wake velocity and  $\bar{V}$  the inlet velocity (time-independent)

$$TI = \frac{100}{\bar{V}} \sqrt{\frac{2}{3}k}$$

with  $k$  is the turbulent kinetic energy

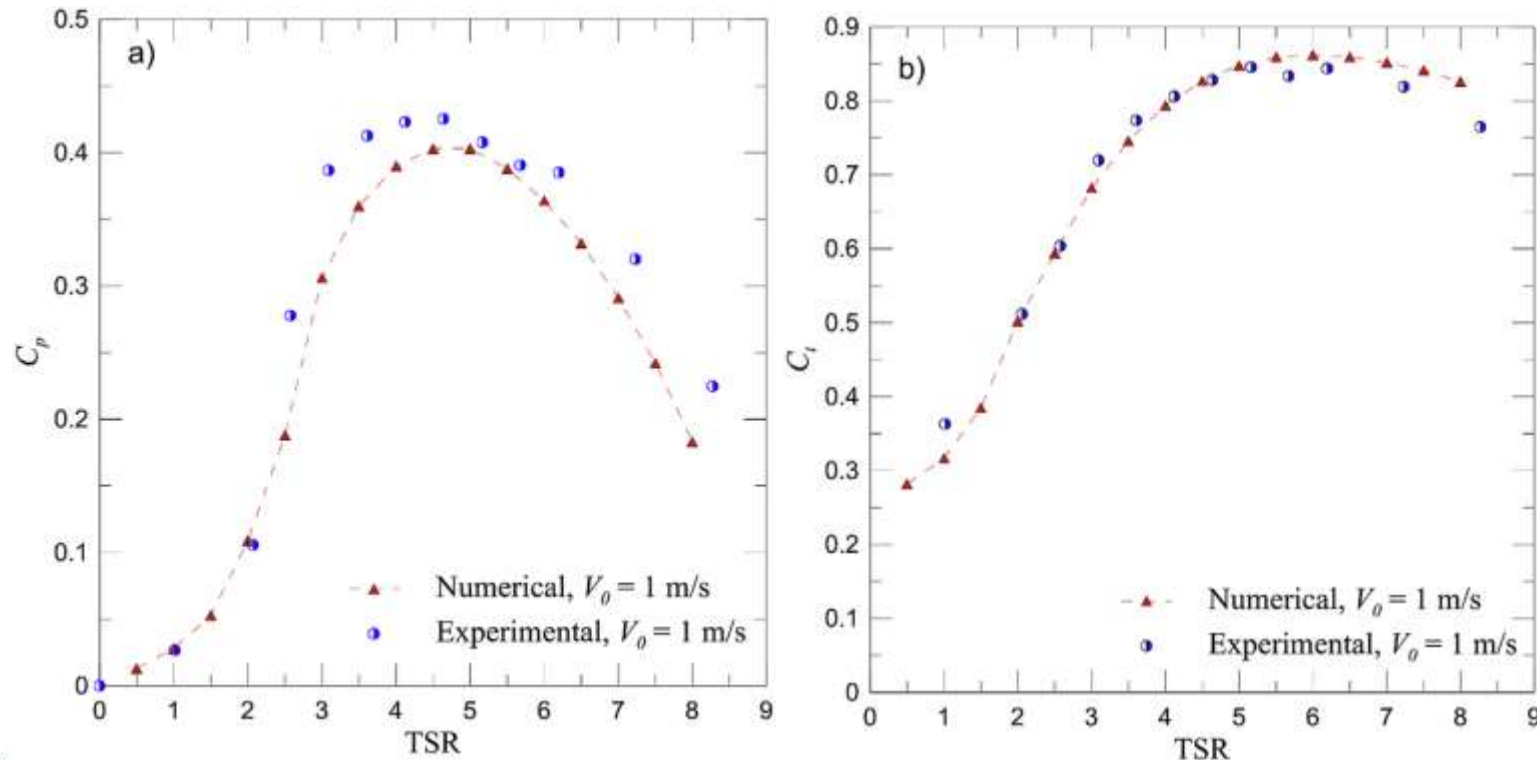
TABLE X Maximum Cell Size in Wake

	Element Size [m]	# of Elements (millions)
Mesh 1	0.22	10.72
Mesh 2	0.11	10.72
Mesh 3	0.055	10.88
Mesh 4	0.0275	12.15
Mesh 5	0.017	16.64
Mesh 6	0.01375	21.69



# Third Geometry and Start of Transient Studies

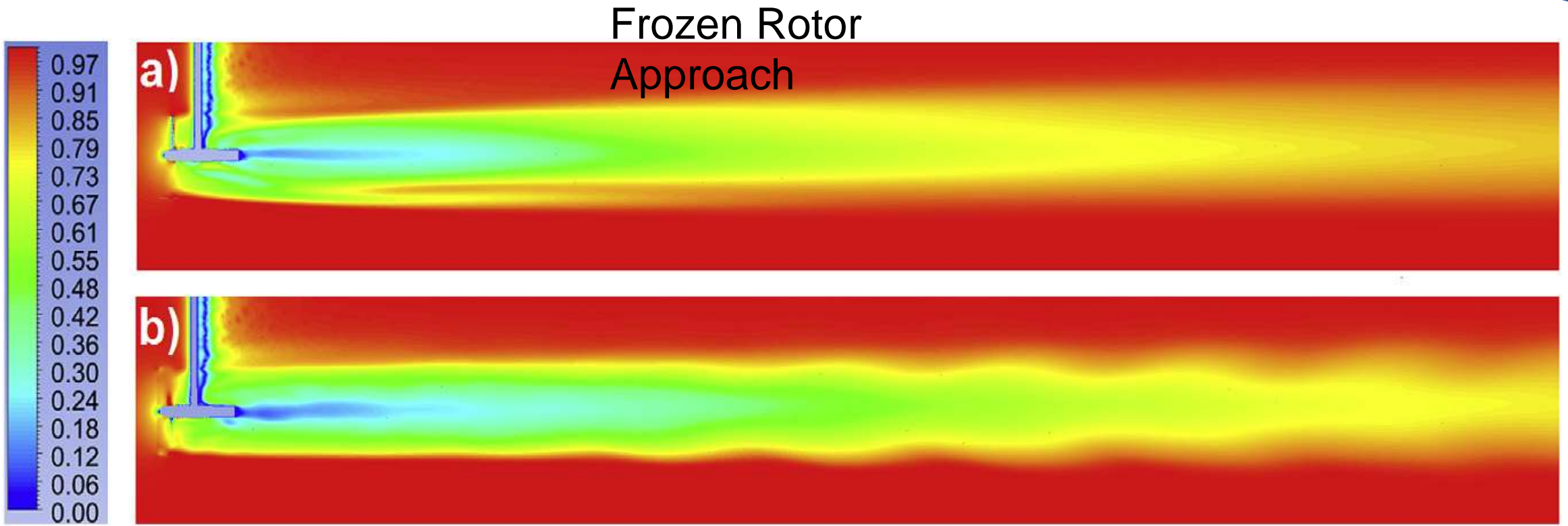
The turbine used by IFREMER, with their accompanied studies where they took measurements in the wake was used to test the difference between the wake results obtained from steady-state or transient numerical studies.



P. Mycek, B. Gaurier, G. Germain, G. Pinon, E. Rivoalen (2014) Experimental study of the turbulence intensity effects on marine current turbines behaviour. Part I: One single turbine, *Renewable Energy*, 66, pp. 729-746



# Normalized Velocity

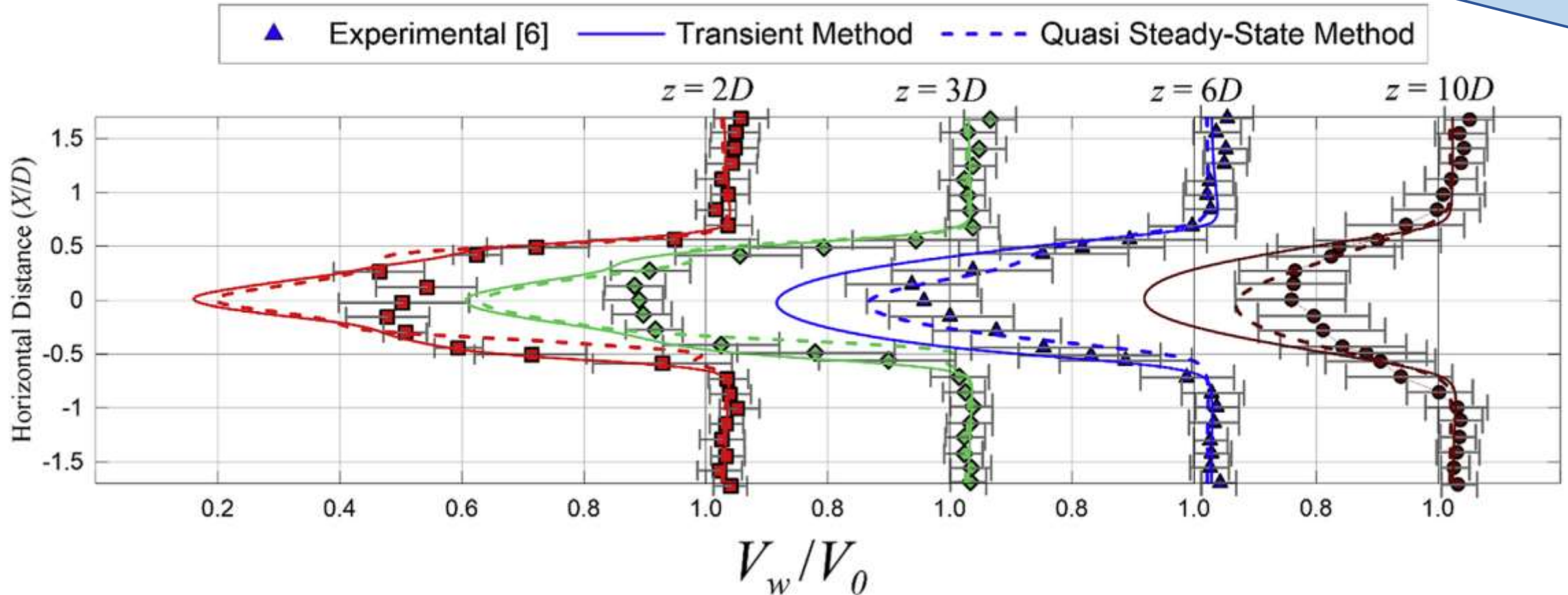


Transient Rotor Approach (snapshot at  $t=80$  s)

T. Leroux, N. Osbourne, D. Groulx, (2019) Numerical study into horizontal tidal turbine wake velocity deficit: Quasi-steady state and transient approaches, *Ocean Engineering*, 181, pp. 240-251



# Comparison to Experimental Data

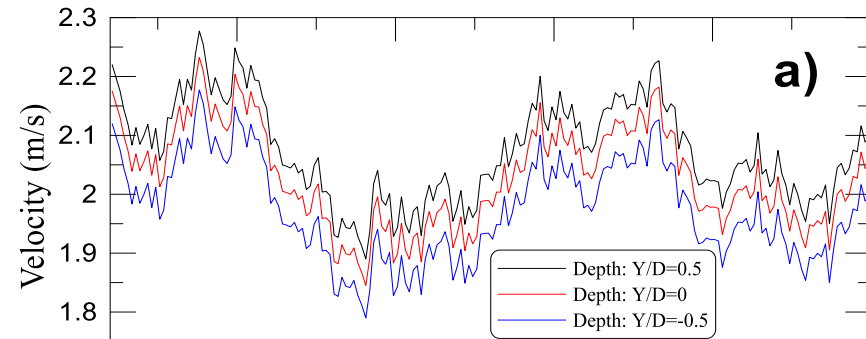


Normalized velocity comparison between IFREMER's experimental results (Mycek et al., 2014) and the quasi steady-state/transient-rotor simulations for distance behind the turbine of  $2D$ ,  $3D$ ,  $6D$  and  $10D$ .  $TSR=3.7$ ,  $I_\infty=3\%$  and  $V_0=0.8$  m/s.

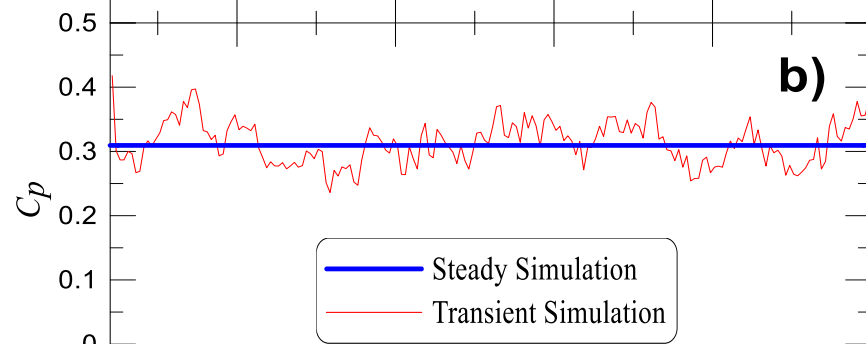


# Transient Simulation Results

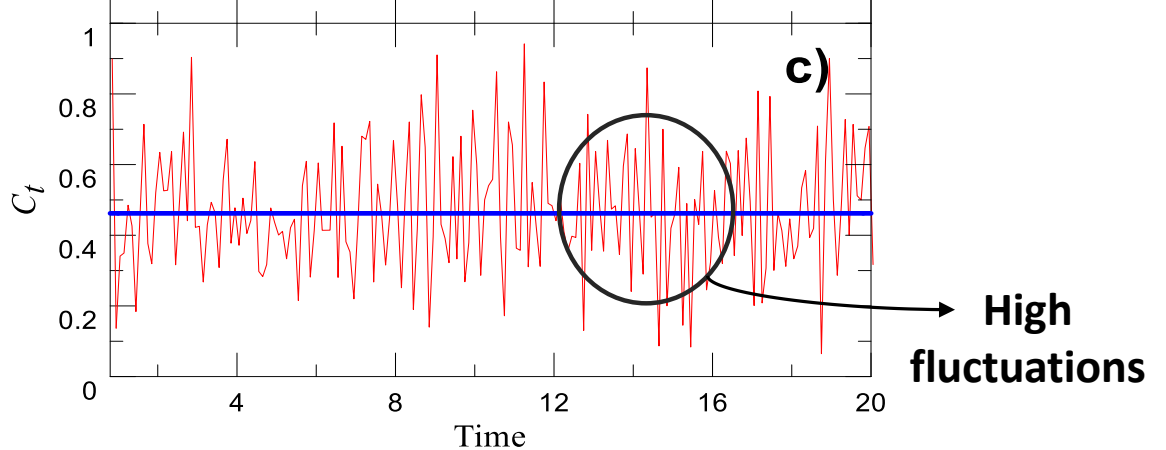
Inlet Velocity as a function of time  
for 3 different depths



Power coefficient  $C_p$  as a function of time

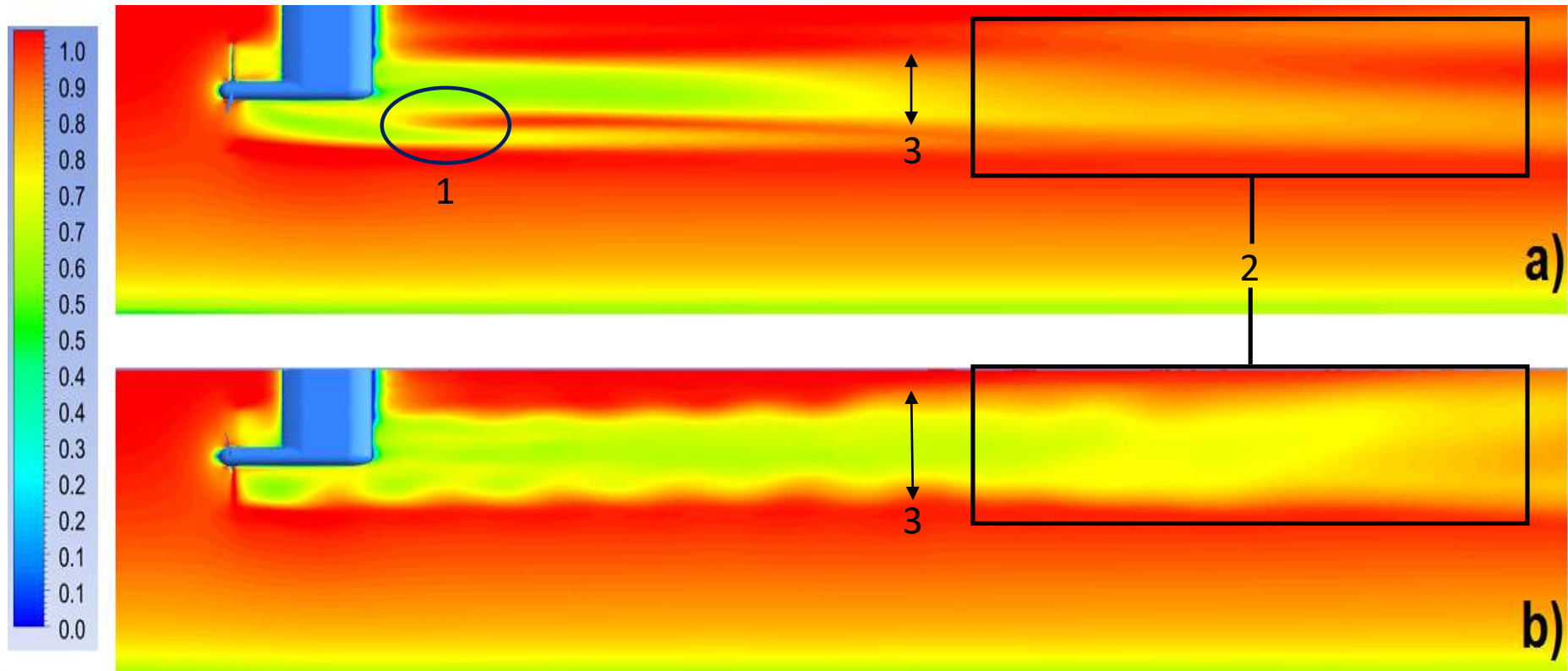


Thrust coefficient  $C_t$  as a function of time



# Wake Characteristics: Velocity Deficit

Normalized Velocity  $V/V_0$  on mid-vertical plane:



Steady case:  
Frozen-Rotor approach

Unsteady case:  
Transient-Rotor approach



# Numerical Domain

*ANSYS CFX*

Fully transient

$k - \omega$  SST  
RANS  
turbulence m

5% Inlet  
Turbulence  
Intensity

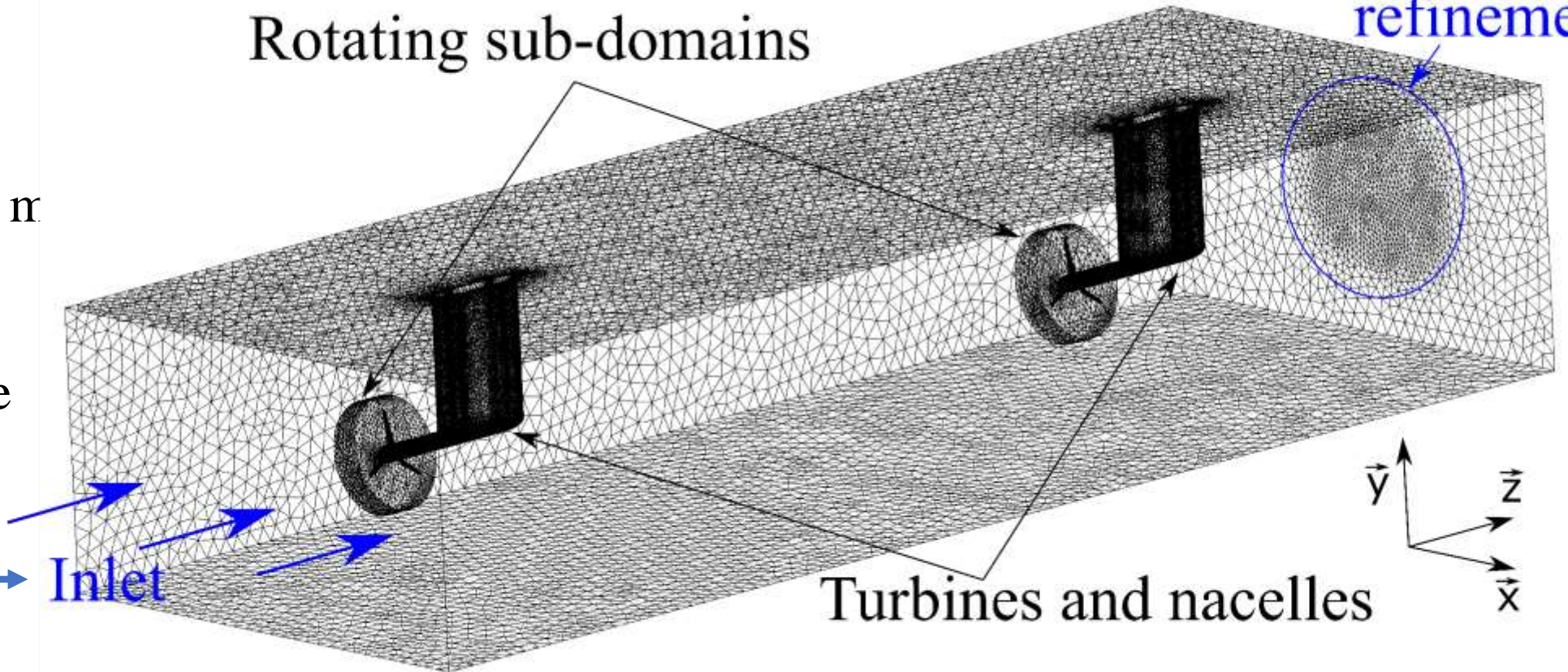
1 m/s

Inlet

Rotating sub-domains

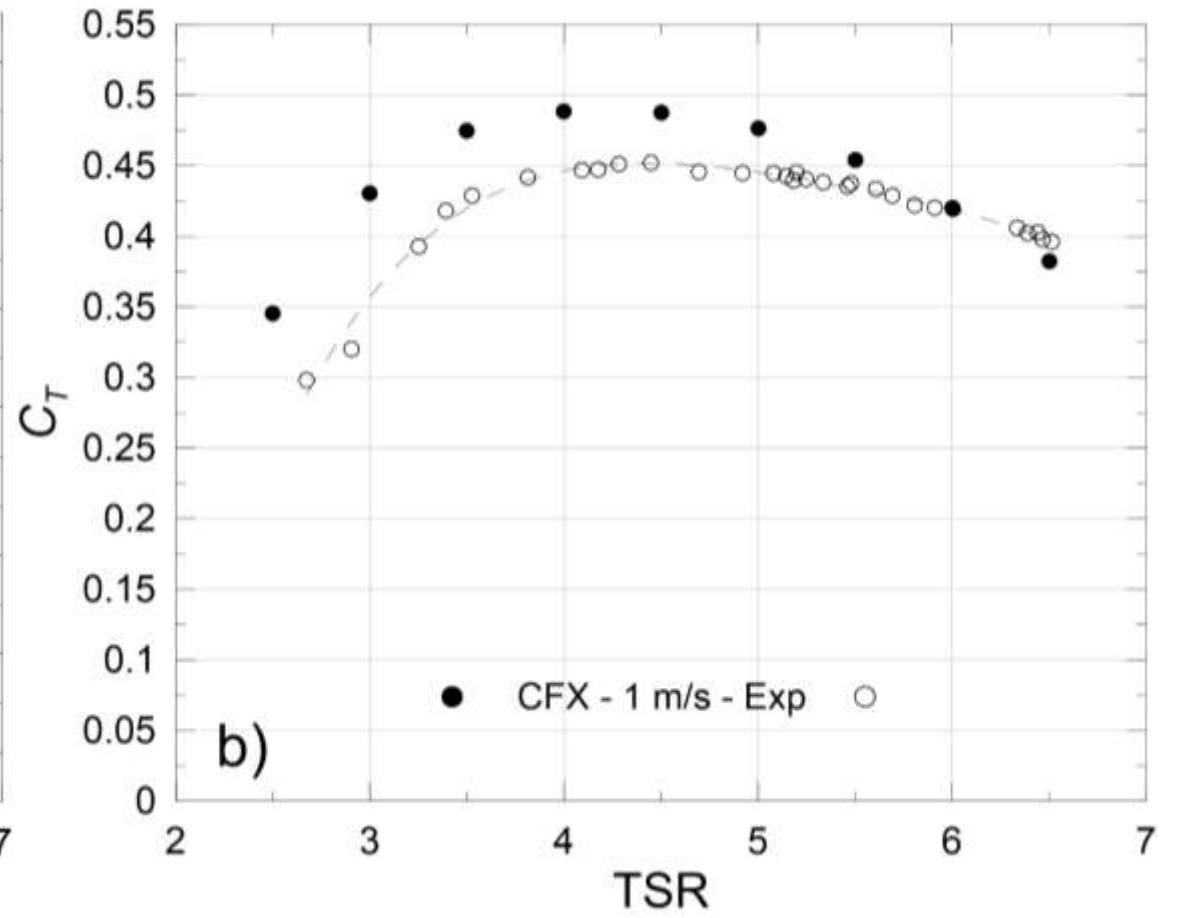
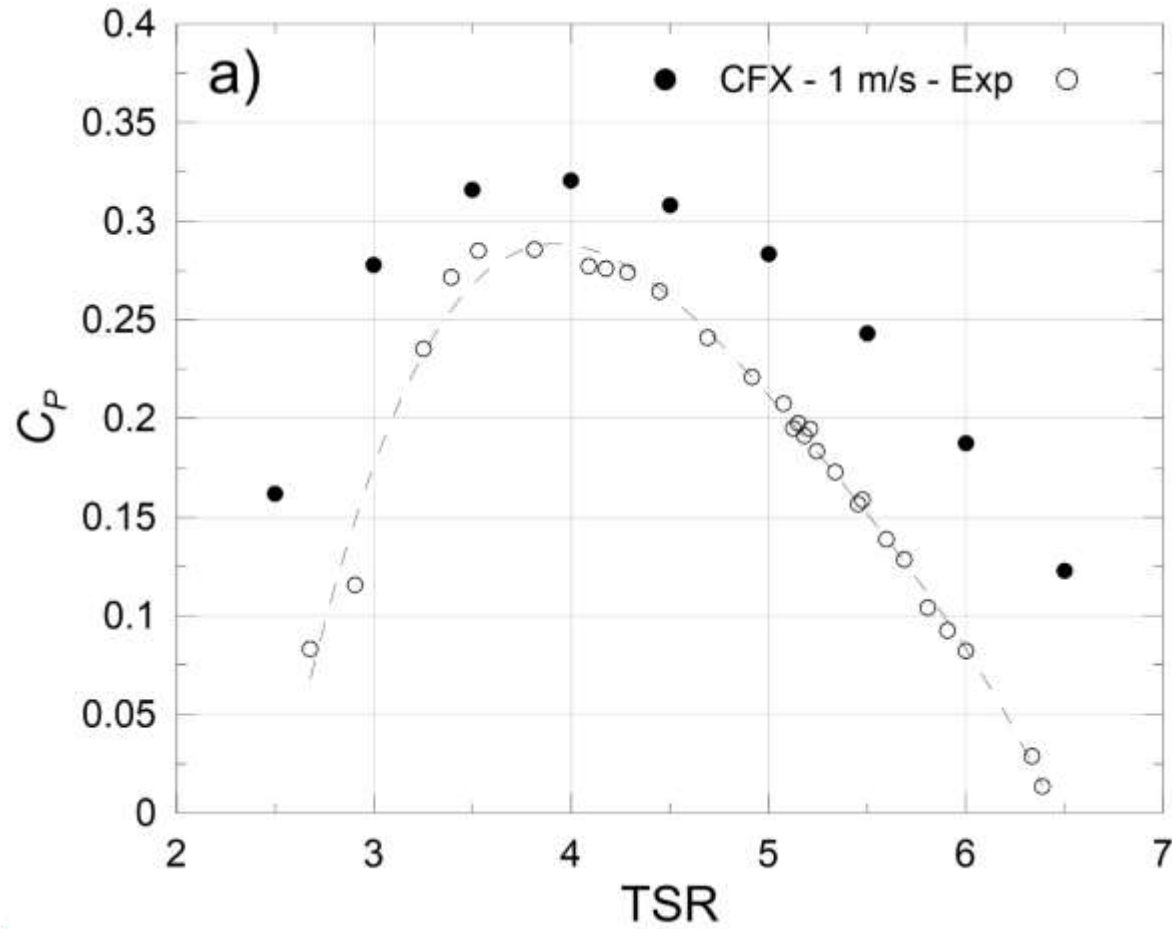
Domain of  
refinement

Turbines and nacelles



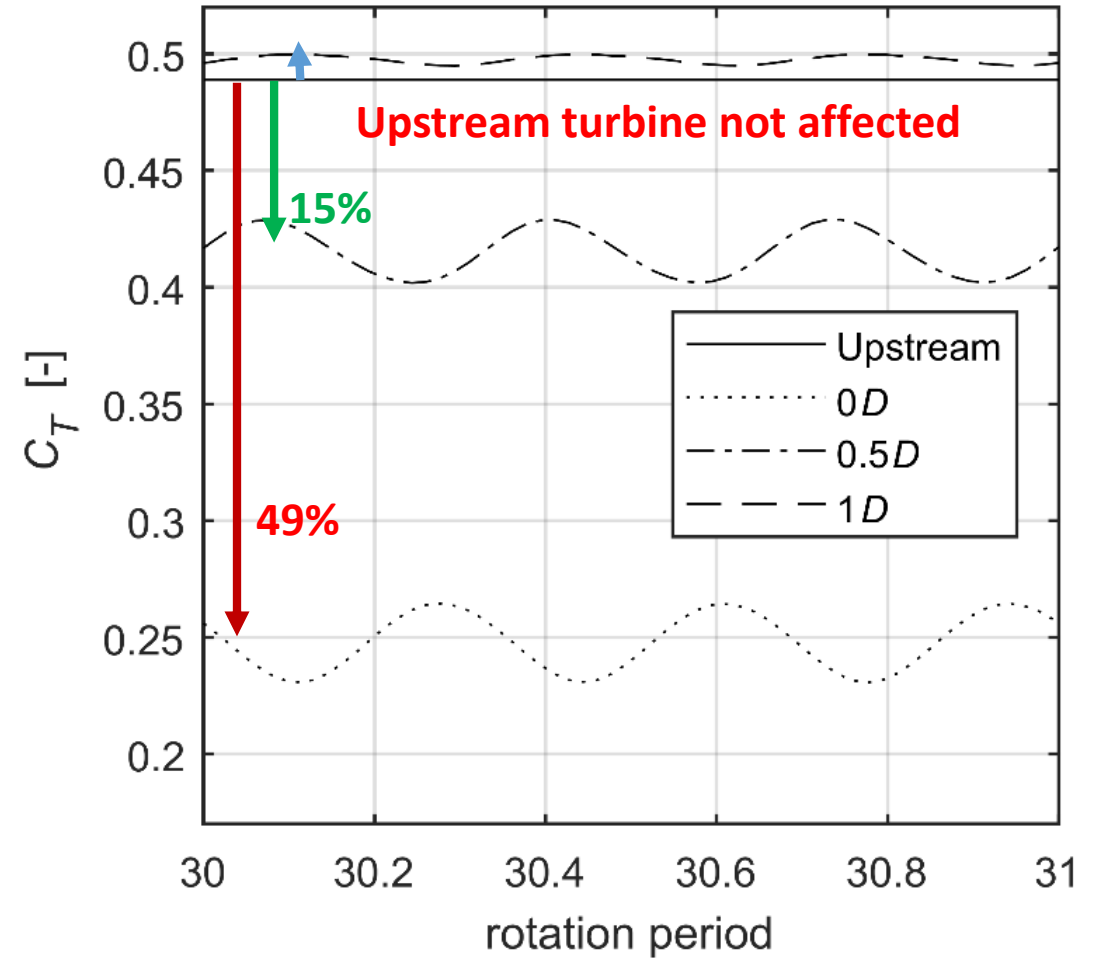
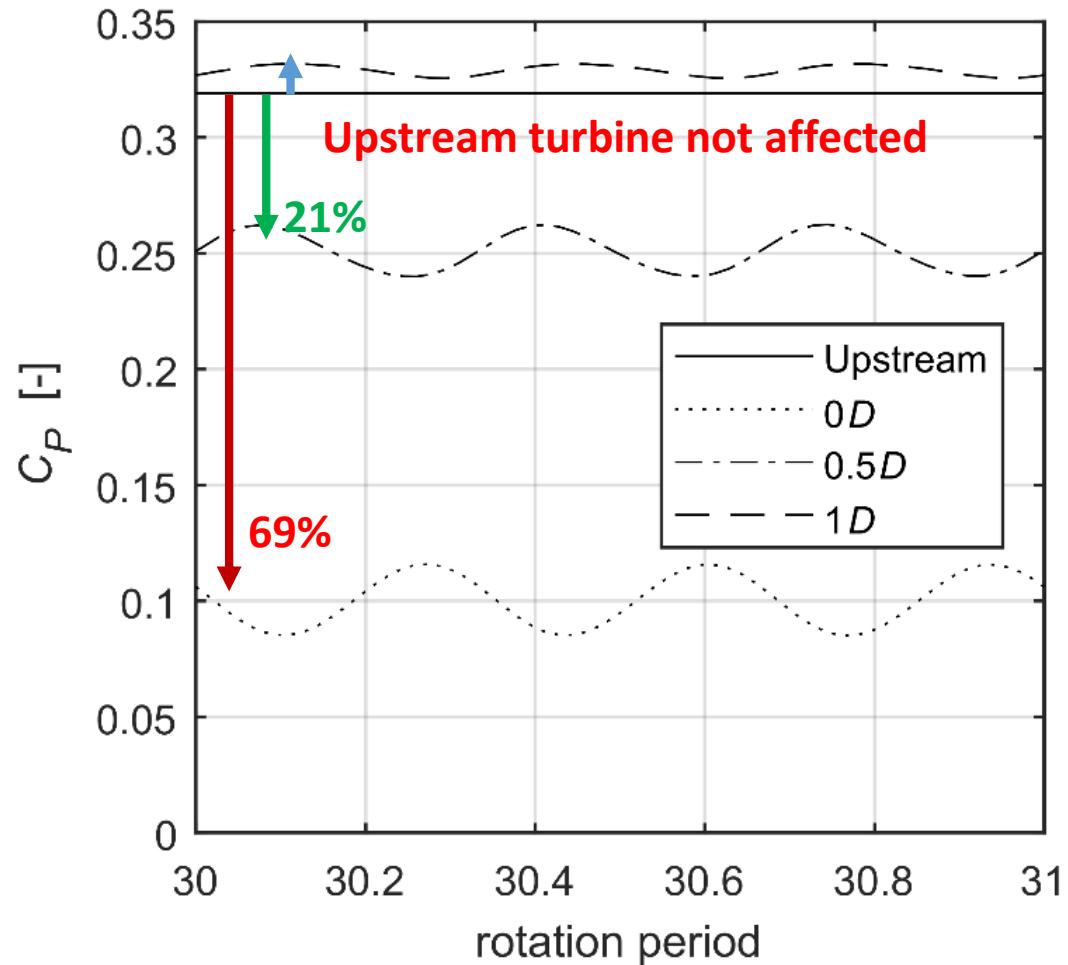


# Comparison to Experimental



# Downstream Turbine Performance

Results at TSR = 4, after a quasi-steady regime is attained

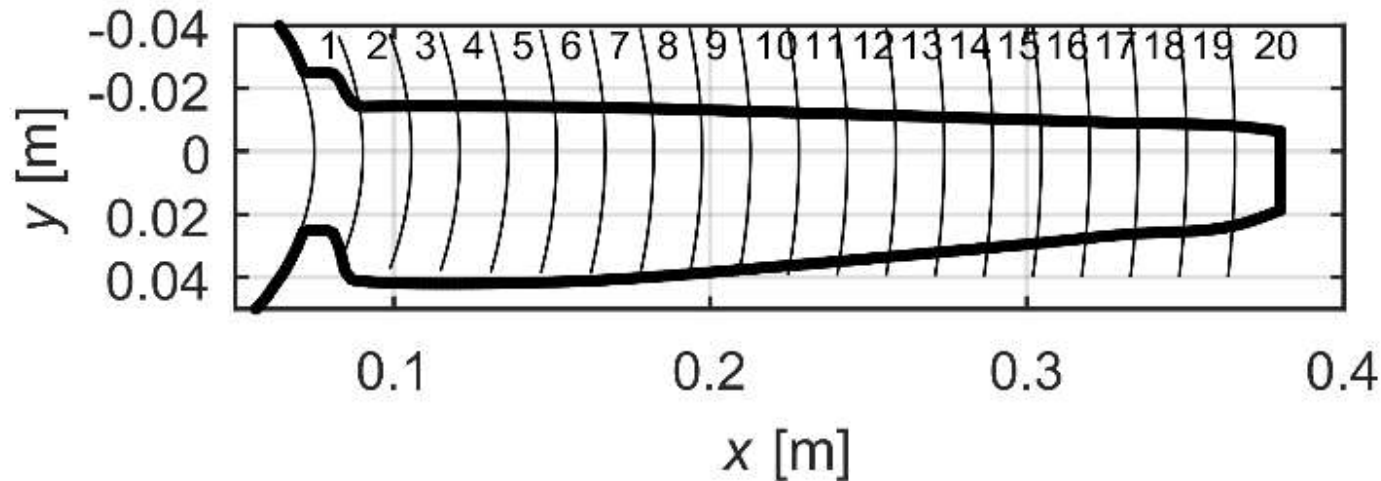


# Downstream Blade Loading

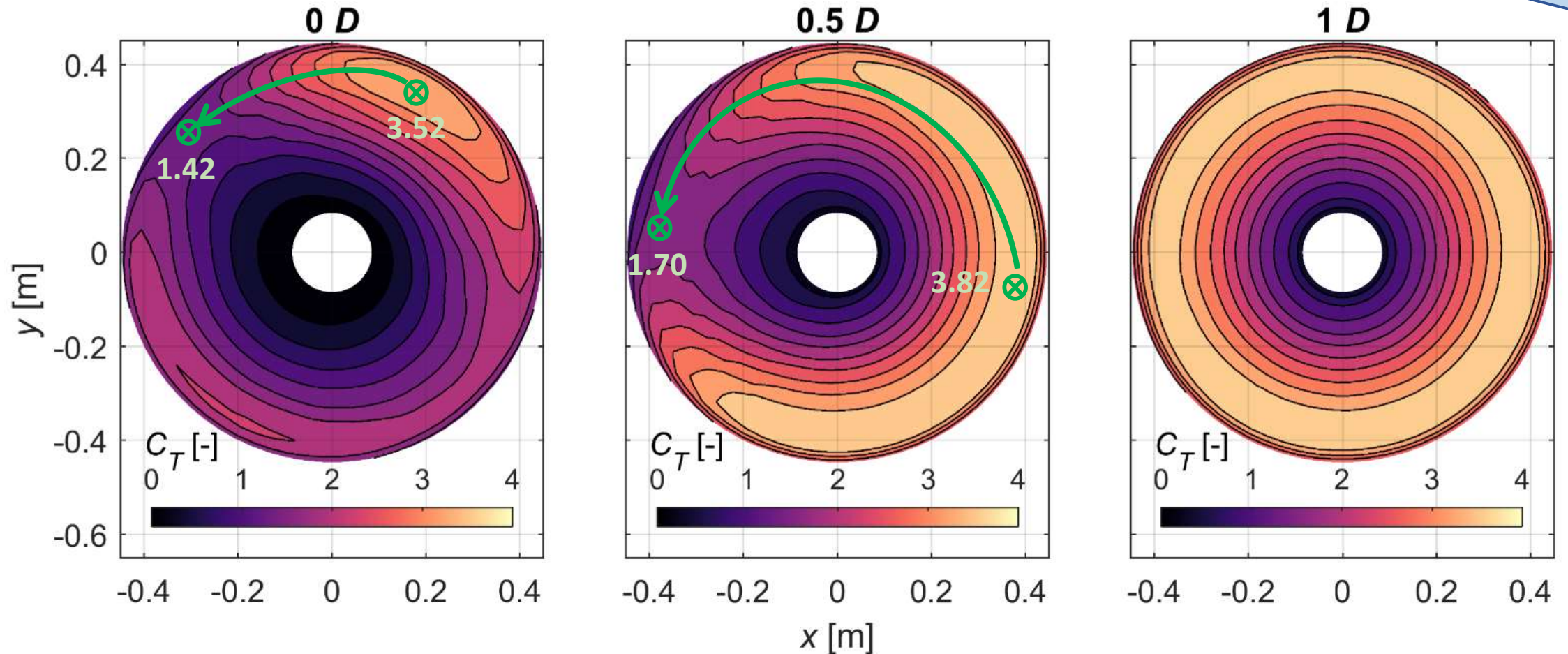
A blade loading map was created to evaluate the load evolution along the blade span with respect to the blade location. The results are presented using a local thrust coefficient:

$$C_{T_l} = \frac{T_l}{\frac{1}{2} \rho_w A_s U_0^2}$$

Evaluated for each blade over a finite number of sections (20).



# Downstream Blade Loading



Values of  $\overline{C_{Tl}}$  over the blade sections over their full rotation range for all three simulated configurations.



# Downstream Blade Loading

