

Subcomponent Validation of Composite Joints for Marine Energy Structures

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## Marine Energy Advanced Materials

- Multiyear, multilaboratory materials research project
- Reduce barriers and uncertainties to adopting advanced composite materials
- Understand environmental effects on complex structures
- Sandia lead laboratory
- NREL subcomponent validation
- MSU material characterization
- PNNL biofouling and coatings
- FAU corrosion.



## **NREL Objectives**

- Address knowledge gaps highlighted in industry surveys and workshops
- Develop subcomponent-scale validation methods for marine energy materials
- Improve understanding of design allowables with environmental degradation of full-scale components and joints
- Reduce the time and cost required for full-scale structural validation
- Provide near-net-scale static and fatigue data on composite subcomponents of materials for marine energy systems.





## **Structural Validation**



- Photo by Paul Murdy, NREL
- ISO 17025 accredited
- Range of test stands
- Hydraulic infrastructure
- State-of-the-art data acquisition, sensor, and non-destructive test equipment.



### Subcomponent Validation





Photo by Taylor Mankle, NREL 67467



## **Project Timeline**

Composite Panels

Thick fiberglass composite panels manufactured at MSU (May 2019) Composite Specimens

Panels manufactured into specimens at NREL (June 2019 to October 2019)

### In-Water Conditioning

Specimens conditioned in ocean water at PNNL and FAU (November 2019 to May 2021)

### Maintaining Conditions

Specimens returned to NREL to await testing (April 2021 to December 2021) Structural Validation

Static and fatigue testing in 500-kN load frame (July 2021 to February 2022)

Photos by Ocean Renewable Power Company 68118, David Miller (MSU), Francisco Presuel-Moreno (FAU), and Paul Murdy (NREL)

## Materials and Manufacturing

- Panels of varying thickness manufactured at MSU
- Vectorply E-QX 9000 E-glass fabric
- Hexion 035c epoxy resin
- Derakane vinylester-epoxy resin
- Vacuum infusion
- Several specimen geometries
- Over 300 specimens in total
- T-Bolt and double-ended-insert (DEI)
- Araldite epoxy and Plexus methylmethacrylate adhesives
- 316 and 2507 stainless steels.



T-Bolt – metal/composite interconnect



Double-Ended-Insert – metal/composite interconnect

Photos by Paul Murdy and Bill Gage, NREL

## Conditioning

- 24 T-Bolt and 14 DEI specimens conditioned
- Dry control specimens remained at NREL
- Half at PNNL under ambient conditions
- Half at FAU at elevated temperatures (58 °C)
- Tracked salinity levels
- 5–18 months
- Returned to cold-water tanks to maintain saturation levels
- Weighed before and after.









Photos by Paul Murdy and Bill Gage, NREL

### Water Absorption Results

- All specimen masses recorded before and after conditioning
- Specimens cleaned, disassembled, and surface water dried prior to weighing
- Some specimens had fiber-optic strain sensors bonded to them throughout the conditioning period.

- Specimens absorbed more water at FAU accelerated aging
- Hexion epoxy T-Bolt specimens absorbed more water than the Derakane vinylester-epoxy specimens
- Water ingress observed deep in DEI bond lines
- Corrosion of 316 steel insert at adhesive interface of DEI only in specimens conditioned at PNNL.



#### DEI Specimens





Photos and images by Paul Murdy and Bill Gage, NREL

## **T-Bolt Static Results**

- Specimens tested in 500-kN load frame with bespoke test fixture
- Aermet 100 ultrahigh-strength studs
- 12 specimens 2 under each environmental condition
- Tensile loading
- All exhibited bearing failures at through-hole
- Derakane generally had higher bearing strengths than Hexion
- All exhibited some degree of environmental degradation
- Hexion degraded more than Derakane at FAU.





Photos and images by Paul Murdy, NREL

## **T-Bolt Fatigue Results**

- Reduced width of specimens due to hardware limitations
- 1–2 specimens under each environmental condition
- Tension-tension, constant amplitude
- All specimens tested at same 130 MPa max tensile stress
- All specimens failed in tension ranging from ~10,000 cycles to ~10,000,000 cycles!
- Dry Hexion epoxy specimens had significantly better fatigue strengths, but suffered severe degradation at FAU
- Derakane vinylester-epoxy specimens had poor fatigue strengths but exhibited little to no degradation.







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## **Double-Ended-Insert Static Results**

- 1–2 specimens per adhesive and insert material combination
- Ultimate shear strengths calculated using insert bonded surface area
- Ultimate shear strength differences were difficult to interpret
- Plexus methyl-methacrylate adhesive did not perform well
- 2507 steel inserts performed better overall
- Observed water deep in bond lines
- Corrosion of 316 steel conditioned at PNNL only.











- Partial saturation can have pronounced effects on larger structures under both static and fatigue loading.
- Conducting fatigue testing at the subcomponent scale can be incredibly timeconsuming and requires detailed project planning to ensure like-for-like comparisons.
- Under the right conditions, there are interactions between 316 steel and adhesives.
- Selecting the correct composite, adhesive, and metals for multimaterial interconnects is a complex process for harsh marine environments.
- The results from this project will help marine energy developers make informed material choices and understand the requirements for evaluating new materials for use in marine structures.
- Full report to be published soon.

## **Future Work**

- Develop models to understand how far water penetrated thick specimens
- Investigate cause of corrosion observed in some 316 steel/adhesive DEI specimens
- Understand synergistic effects of water/fatigue/temperature
- Develop models to support synergistic testing
- Continue to explore other commonly used composites and future materials.



# Thank You

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